Mathematical Aspects of Object-Oriented Modeling and Simulation

5th International Modelica Conference
Wien

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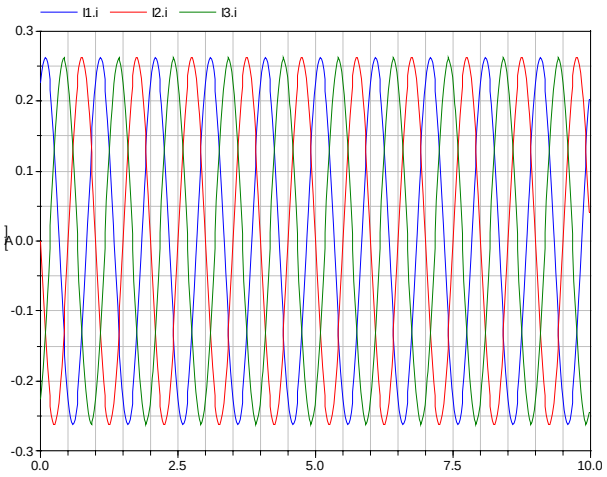
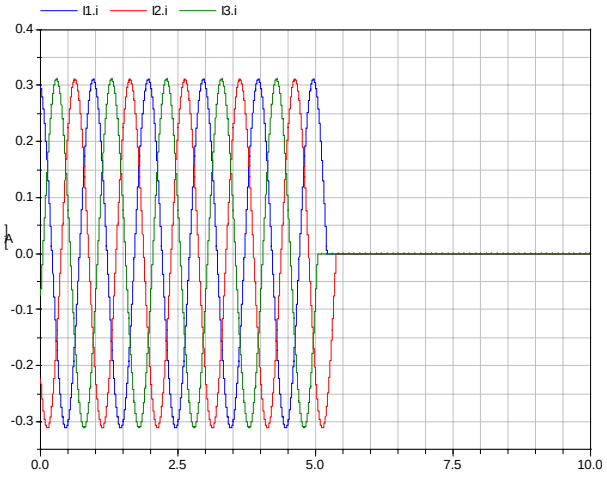
Outline

- Continuous system simulation
  - Introductory example
  - Symbolic transformation
  - Efficiency issues and non-linearities
  - Higher index problems
  - Initialization
  - Numerical issues

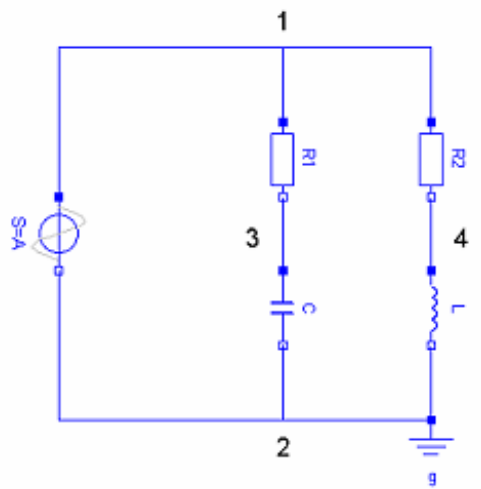


- Mixed system simulation
  - Event handling
  - State events ⇔ time events
  - Symbolic transformation
  - Ideal components
  - Varying higher index problems
  - Efficiency and numerical issues

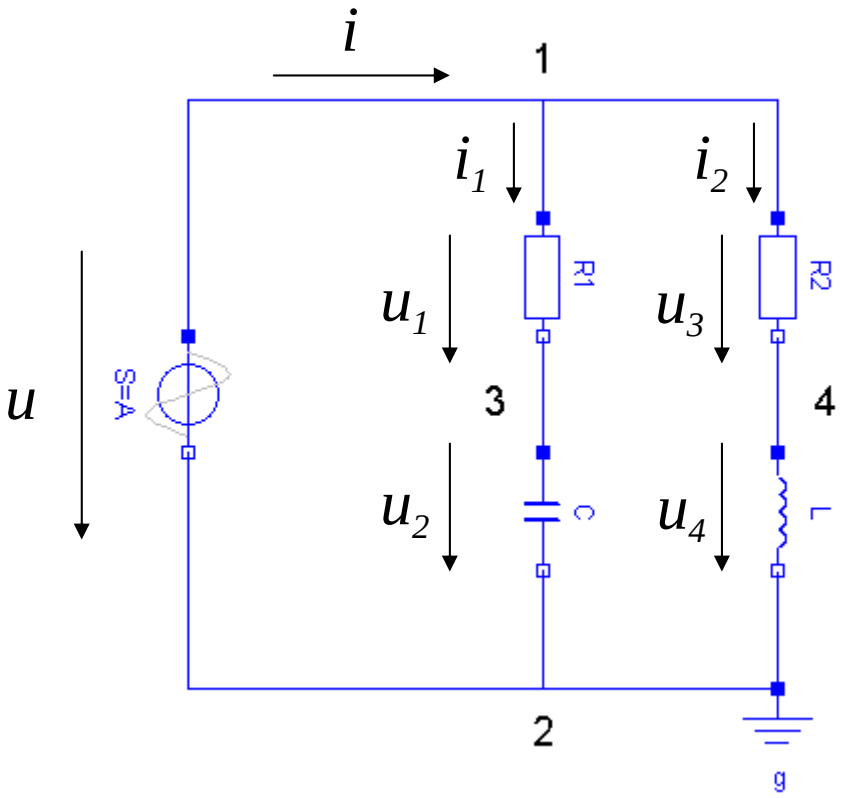


Introductory Example

- Flat model description
  - Differential equations, algebraic equations
  - Parameters, constants, and continuous variables
- Mathematical formalism
  - Differential-algebraic equations (DAEs)
  - Principles of numerical solution methods
  - Same number of equations and unknowns
  - Basic transformation steps
  - Explicit state-space representation
- Hierarchical modeling
  - Local description by equations
  - Connection equations describe interaction
  - Elimination of trivial equations
  - Explicit state-space representation



Example: A Simple Electrical System
Flat Representation



$$u = A \cdot \sin(\omega\, t)$$

$$u = u_1 + u_2, \quad u = u_3 + u_4$$

$$i = i_1 + i_2$$

$$u_1 = R_1 i_1, \quad u_3 = R_2 i_2,$$

$$C\frac{du_2}{dt} = i_1, \quad L\frac{di_2}{dt} = u_4$$

The dynamical behavior of the system is given by a

System of differential-algebraic equations (DAEs)

Mathematical Formalism

General representation of DAEs:

$$\underline{0} = \underline{f}\left(t,\ \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

t	time
$\underline{\dot{x}}(t)$	vector of differentiated state variables
$\underline{x}(t)$	vector of state variables
$\underline{y}(t)$	vector of algebraic variables
$\underline{u}(t)$	vector of input variables
$\underline{p}$	vector of parameters and/or constants

Example: A Simple Electrical System

Model of the electrical system:

$$u = A \cdot \sin(\omega\, t + \varphi)$$

$$u = u_1 + u_2, \quad u = u_3 + u_4$$

$$i = i_1 + i_2$$

$$u_1 = R_1\ i_1, \quad u_3 = R_2\ i_2$$

$$C\ \dot{u}_2 = i_1, \quad L\ \dot{i}_2 = u_4$$

- 8 equations!
- Number of unknowns?
- Solution of the system?

General representation:

$$\underline{0} = \underline{f}\left(t,\ \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

t time, $\underline{\dot{x}}(t) = \begin{pmatrix} \dot{u}_2 \\ \dot{i}_2 \end{pmatrix}$, $\underline{x}(t) = \begin{pmatrix} u_2 \\ i_2 \end{pmatrix}$,

$$\underline{y}(t) = \begin{pmatrix} u \\ u_1 \\ u_3 \\ u_4 \\ i \\ i_1 \end{pmatrix}, \quad \underline{u}(\mathrm{t}) \text{ not present}, \quad \underline{p} = \begin{pmatrix} A \\ \omega \\ R_1 \\ R_2 \\ C \\ L \end{pmatrix}$$

Understand Numerical Integration Methods (Explicit Euler Method)

Integration of explicit ordinary differential equations (ODEs):

$$\dot{\underline{x}}(t) = \underline{f}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right), \qquad \underline{x}(t_0) = \underline{x}_0$$

Numerical approximation of the derivative and/or right-hand-side:

$$\dot{\underline{x}}(t_n) \approx \frac{\underline{x}(t_{n+1}) - \underline{x}(t_n)}{t_{n+1} - t_n} \approx \underline{f}\left(t_n, \underline{x}(t_n), \underline{u}(t_n), \underline{p}\right)$$

Iteration scheme:

$$\underline{x}(t_{n+1}) \approx \underline{x}(t_n) + \left(t_{n+1} - t_n\right) \cdot \underline{f}\left(t_n, \underline{x}(t_n), \underline{u}(t_n), \underline{p}\right)$$

Convergence?

Calculating an approximation of $\underline{x}(t_{n+1})$ based on the values of $\underline{x}(t_n)$

Here:
Explicit Euler integration method

Basic Transformation Steps

Transformation to explicit state-space representation:

$$\underline{0} = \underline{f}\left(t, \dot{\underline{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

$$\underline{z}(t) = \begin{pmatrix} \dot{\underline{x}}(t) \\ \underline{y}(t) \end{pmatrix} = \underline{g}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\underline{0} = \underline{f}\left(t, \underline{z}(t), \underline{x}(t), \underline{u}(t), \underline{p}\right), \quad \underline{z}(t) = \begin{pmatrix} \dot{\underline{x}}(t) \\ \underline{y}(t) \end{pmatrix}$$

$$\dot{\underline{x}}(t) = \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\underline{y}(t) = \underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

Implicit function theorem:

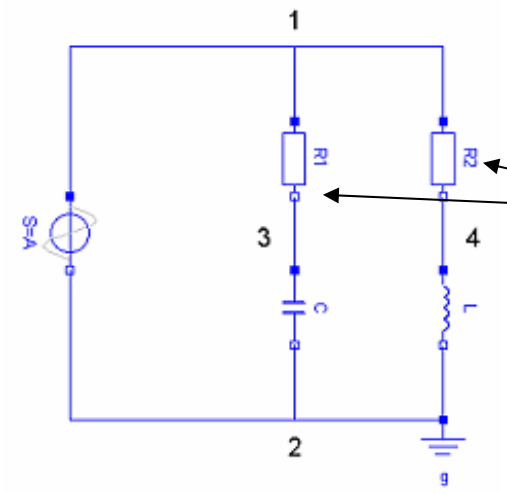
Necessary condition for the existence of the transformation is that the following matrix is regular at the point of interest:

$$\det\left(\frac{\partial}{\partial \underline{z}} \underline{f}\left(t, \underline{z}(t), \underline{x}(t), \underline{u}(t), \underline{p}\right)\right) \neq 0$$

Example: A Simple Electrical System

Model of the electrical system:

$$u = A \cdot \sin(\omega\, t)$$
$$u = u_1 + u_2, \quad u = u_3 + u_4, \quad i = i_1 + i_2$$
$$u_1 = R_1 i_1, \quad u_3 = R_2 i_2$$
$$C\dot{u}_2 = i_1, \quad L\dot{i}_2 = u_4$$



Causality!

Transformation to explicit state space representation:

$$u = A \cdot \sin(\omega\, t)$$
$$u_3 = R_2 i_2$$
$$u_1 = u - u_2$$
$$u_4 = u - u_3$$
$$i_1 = u_1 / R_1$$
$$i = i_1 + i_2$$
$$\dot{u}_2 = i_1 / C$$
$$\dot{i}_2 = u_4 / L$$

Transformed Simulation Model

Model of the electrical system in explicit state space representation:

$$u = A \cdot \sin(\omega\, t)$$
$$u_3 = R_2 i_2$$
$$u_1 = u - u_2$$
$$u_4 = u - u_3$$
$$i_1 = u_1 / R_1$$
$$i = i_1 + i_2$$
$$\dot{u}_2 = i_1 / C$$
$$\dot{i}_2 = u_4 / L$$

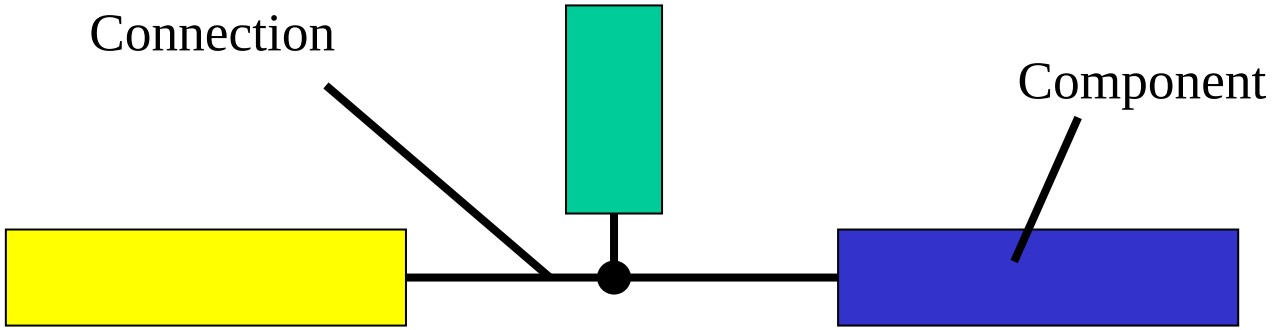
General representation:

$$\dot{\underline{x}}(t) = \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$
$$\underline{y}(t) = \underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\begin{pmatrix} \dot{u}_2(t) \\ \dot{i}_2(t) \end{pmatrix} = \underline{h}\left(t, \underbrace{u_2(t), i_2(t)}_{\text{states}}, \underbrace{A, \omega, R_1, R_2, C, L}_{\text{parameters/constants}}\right)$$

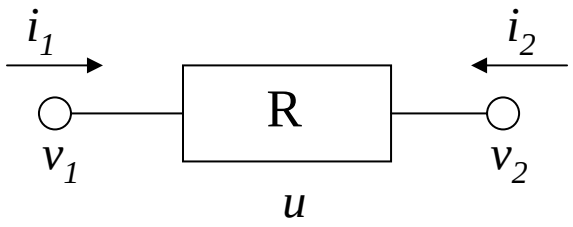
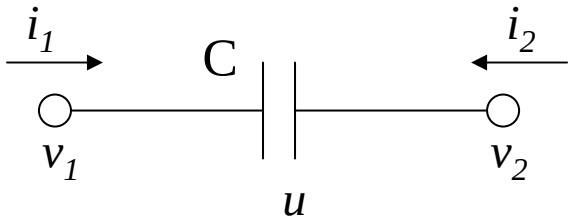
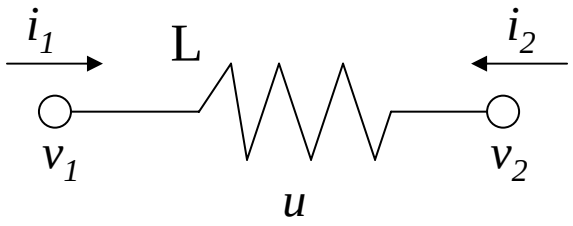
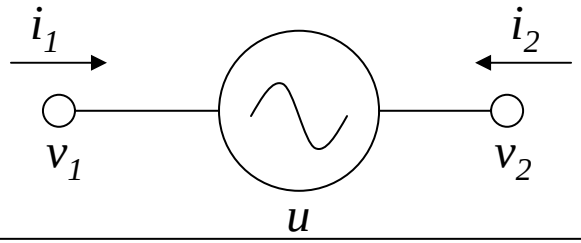
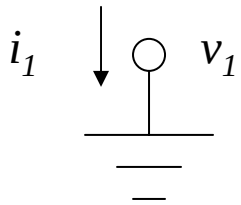
$$\begin{pmatrix} u(t) \\ u_1(t) \\ u_3(t) \\ u_4(t) \\ i(t) \\ i_1(t) \end{pmatrix} = \underline{k}\left(t, \underbrace{u_2(t), i_2(t)}_{\text{states}}, \underbrace{A, \omega, R_1, R_2, C, L}_{\text{parameters/constants}}\right)$$

Hierarchical Object-Oriented Modeling



- Each icon represents a physical component
  - Electrical resistor, mechanical gearbox, pump
- Composition lines are the actual physical connections
  - Electrical line, mechanical connection,
    heat flow between two components
- Variables at the interfaces describe interaction with other components
- Physical behavior of a component is described by equations
- Hierarchical decomposition of components

Hierarchical Model of the Electrical System

Resistor		$0 = i_1 + i_2$ $u = v_1 - v_2$ $u = R\ i_1$
Capacitor		$0 = i_1 + i_2$ $u = v_1 - v_2$ $i_1 = C\ du/dt$
Inductor		$0 = i_1 + i_2$ $u = v_1 - v_2$ $u = L\ di_1/dt$
Voltage source		$0 = i_1 + i_2$ $u = v_1 - v_2$ $u = A\ sin(wt)$
Ground		$v_1 = 0$

Hierarchical Model of the Electrical System

R1

$0 = R1.i_1 + R1.i_2$

$R1.u = R1.v_1 - R1.v_2$

$R1.u = R1.R \cdot R1.i_1$

R2

$0 = R2.i_1 + R2.i_2$

$R2.u = R2.v_1 - R2.v_2$

$R2.u = R2.R \cdot R2.i_1$

C

$0 = C.i_1 + C.i_2$

$C.u = C.v_1 - C.v_2$

$C.i_1 = C.C \cdot dC.u/dt$

L

$0 = L.i_1 + L.i_2$

$L.u = L.v_1 - L.v_2$

$L.u = L.L \cdot dL.i_1/dt$

S

$0 = S.i_1 + S.i_2$

$S.u = S.v_1 - S.v_2$

$S.u = S.A \sin(S.w \cdot t)$

g

$g.v_1 = 0$

1

$S.v_1 = R1.v_1$

$S.v_1 = R2.v_1$

$0 = S.i_1 + R1.i_1 + R2.i_1$

3

$R1.v_2 = C.v_1$

$0 = R1.i_2 + C.i_1$

2

$g.v_1 = C.v_2$

$g.v_1 = L.v_2$

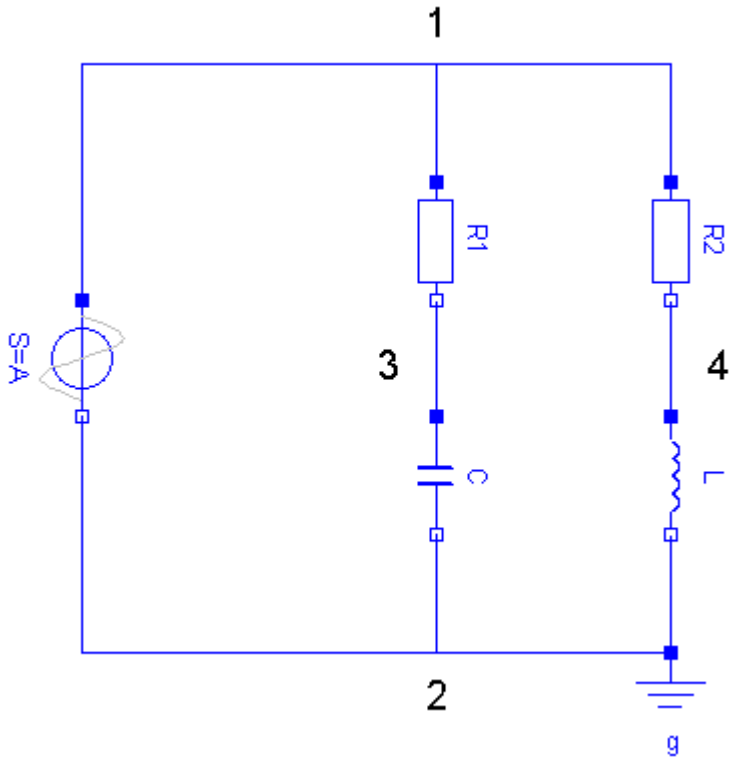
$g.v_1 = S.v_2$

$0 = g.i_1 + C.i_2 + L.i_2 + S.i_2$

4

$R2.v_2 = L.v_1$

$0 = R2.i_2 + L.i_1$

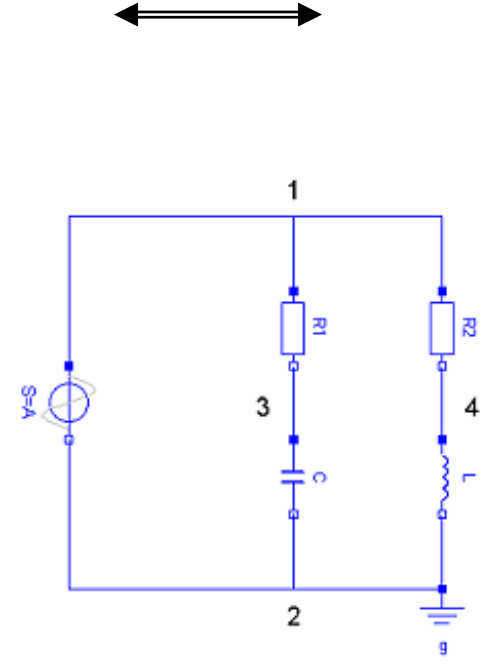


- 27 equations!
- number of unknowns?
- many trivial equations!

Hierarchical Model of the Electrical System

Transformation to explicit state space representation with elimination of trivial equations and further simplifications

$$
\begin{aligned}
R1.v_1 &:= S.A \cdot \sin(S.w \cdot t) \\
R2.u &:= R2.R \cdot L.i_1 \\
R1.u &:= R1.v_1 - C.u \\
L.u &:= R1.v_1 - R2.u \\
C.i_1 &:= R1.u / R1.R \\
S.i_1 &:= C.i_1 + L.i_1 \\
dC.u/dt &:= C.i_1 / C.C \\
dL.i_1/dt &:= L.u / L.L
\end{aligned}
$$



$$
\begin{aligned}
u &= A \cdot \sin(\omega\, t) \\
u_3 &= R_2 i_2 \\
u_1 &= u - u_2 \\
u_4 &= u - u_3 \\
i_1 &= u_1 / R_1 \\
i &= i_1 + i_2 \\
\dot{u}_2 &= i_1 / C \\
\dot{i}_2 &= u_4 / L
\end{aligned}
$$

Symbolic Transformation Algorithmic Steps

- DAEs and bipartite graph representation
  - Structural representation of the equation system
- The matching problem
  - Assign to each variable exact one equation
  - Same number of equations and unknowns
- Construct a directed graph
  - Find sinks, sources and strong components
  - Sorting the equation system
- Adjacence Matrix and structural regularity
  - Block-lower triangular form (BLT-Transformation)

$$\underline{0} = \underline{f}\left(t, \dot{\underline{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

$$\downarrow$$

$$\underline{0} = \underline{f}\left(t, \underline{z}(t), \underline{x}(t), \underline{u}(t), \underline{p}\right), \quad \underline{z}(t) = \begin{pmatrix} \dot{\underline{x}}(t) \\ \underline{y}(t) \end{pmatrix}$$

$$\downarrow$$

$$\underline{z}(t) = \begin{pmatrix} \dot{\underline{x}}(t) \\ \underline{y}(t) \end{pmatrix} = \underline{g}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\downarrow$$

$$\dot{\underline{x}}(t) = \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\underline{y}(t) = \underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

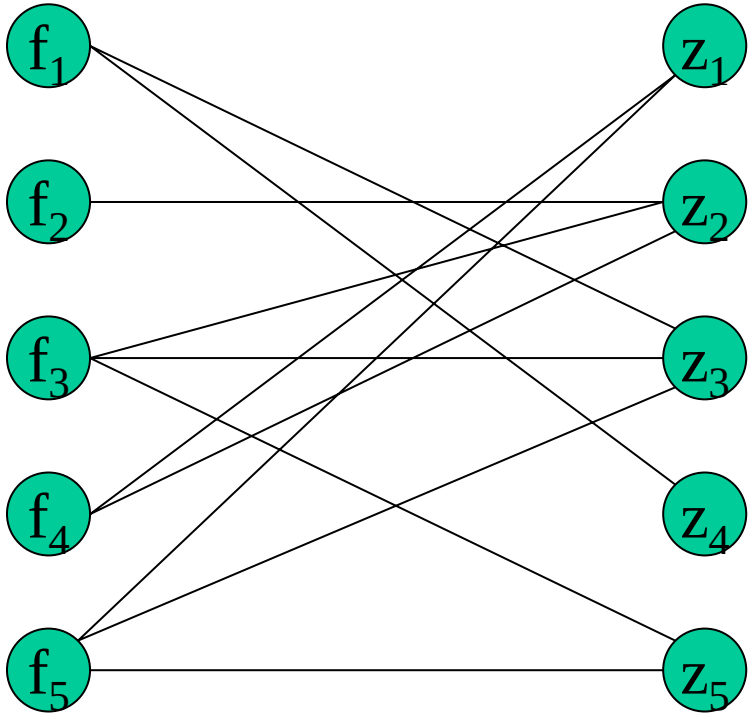
DAEs and Bipartite Graph Representation

Example of a regular DAE:

$$\underline{0} = \underline{f}\left(t, \underline{z}(t), \underline{x}(t), \underline{u}(t), \underline{p}\right), \quad \underline{z}(t) = \begin{pmatrix} \underline{\dot{x}}(t) \\ \underline{y}(t) \end{pmatrix}$$

$$\begin{aligned} f_1(z_3,z_4) &= 0 \\ f_2(z_2) &= 0 \\ f_3(z_2,z_3,z_5) &= 0 \\ f_4(z_1,z_2) &= 0 \\ f_5(z_1,z_3,z_5) &= 0 \end{aligned}$$

Bipartite graph



Adjacence matrix

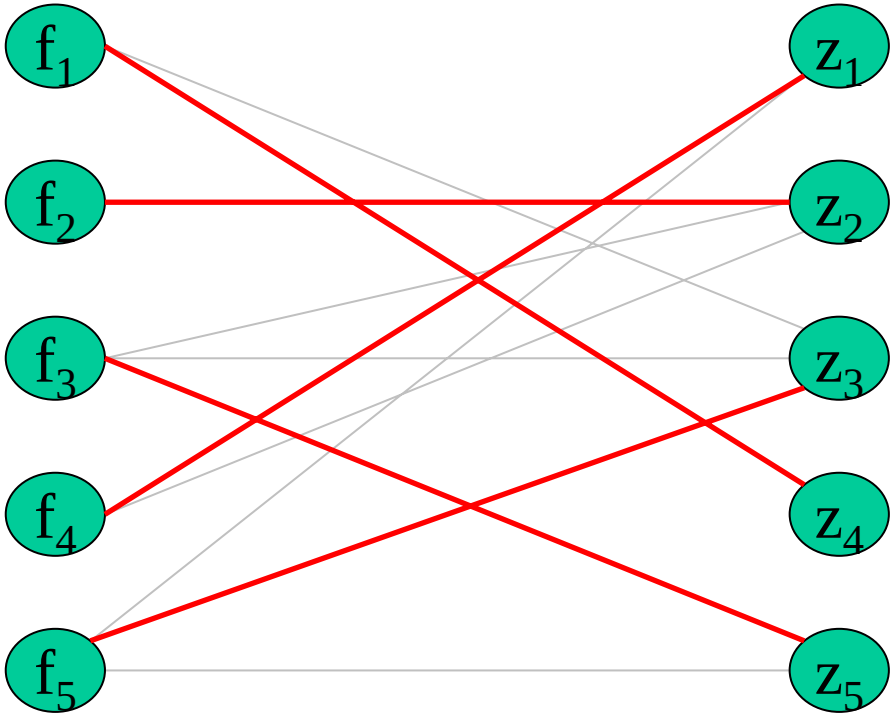
	z_1	z_2	z_3	z_4	z_5
f_1	0	0	1	1	0
f_2	0	1	0	0	0
f_3	0	1	1	0	1
f_4	1	1	0	0	0
f_5	1	0	1	0	1

Solve the Matching Problem

Example of a regular DAE:

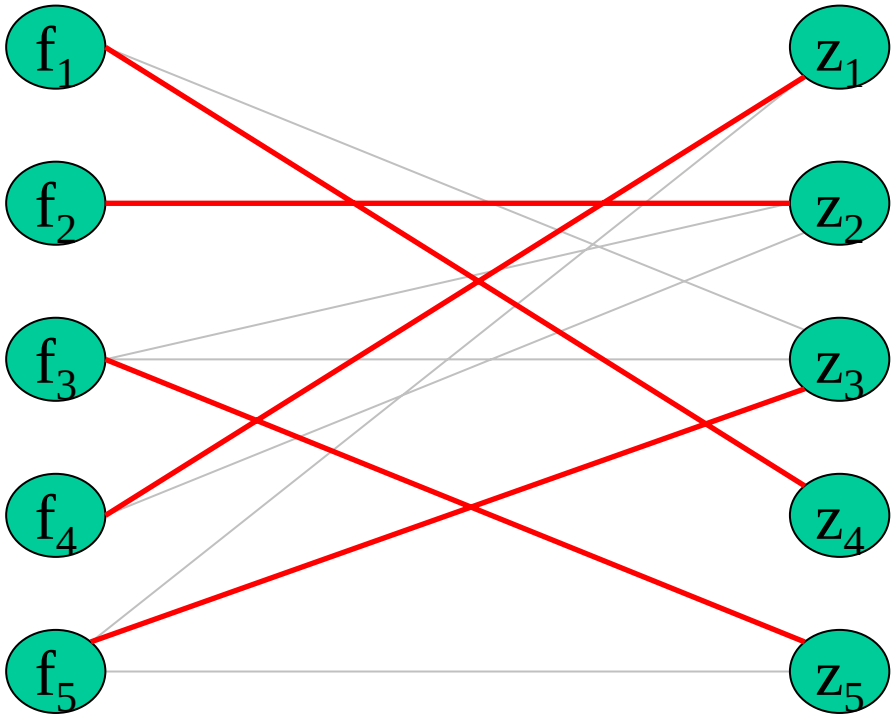
$$
\begin{aligned}
f_1(z_3,z_4) &= 0\\
f_2(z_2) &= 0\\
f_3(z_2,z_3,z_5) &= 0\\
f_4(z_1,z_2) &= 0\\
f_5(z_1,z_3,z_5) &= 0
\end{aligned}
$$

Bipartite graph

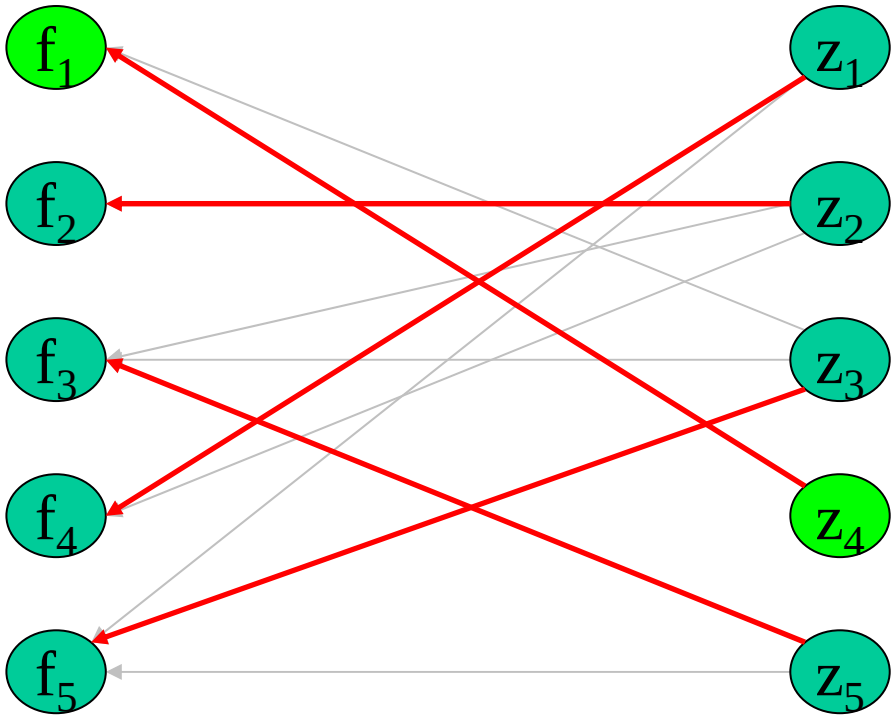


	z_1	z_2	z_3	z_4	z_5
f_1	0	0	1	**1**	0
f_2	0	**1**	0	0	0
f_3	0	1	1	0	**1**
f_4	**1**	1	0	0	0
f_5	1	0	**1**	0	1

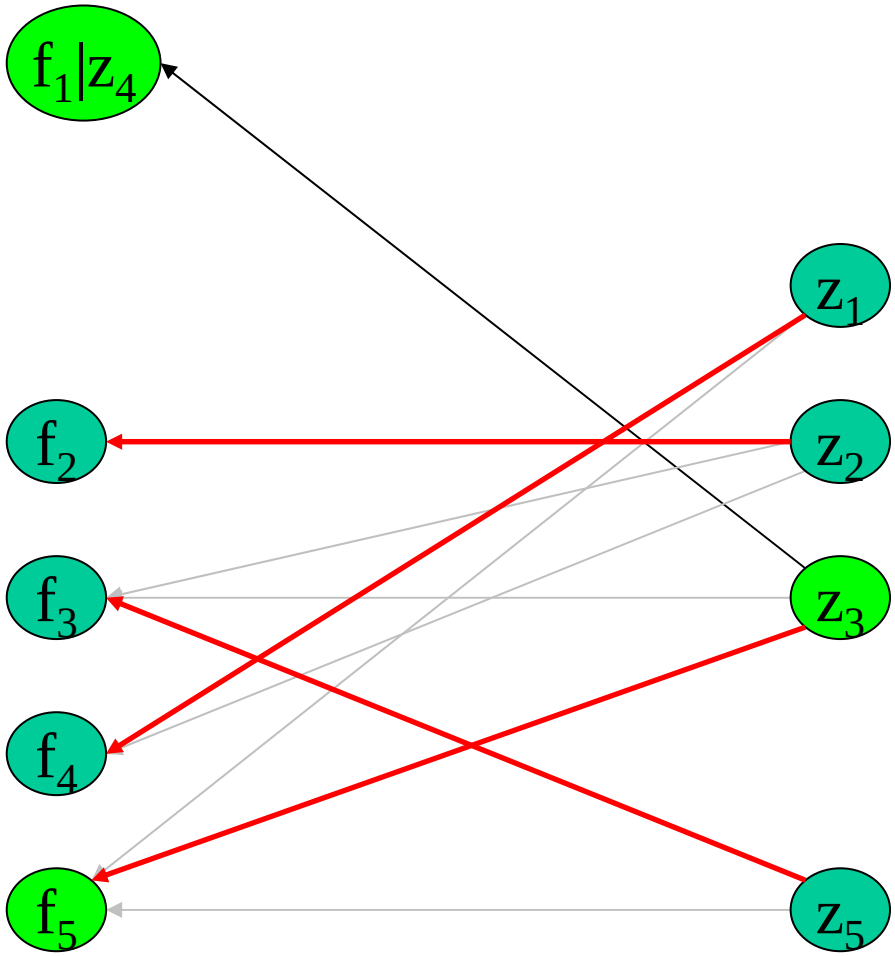
Construct a Directed Graph



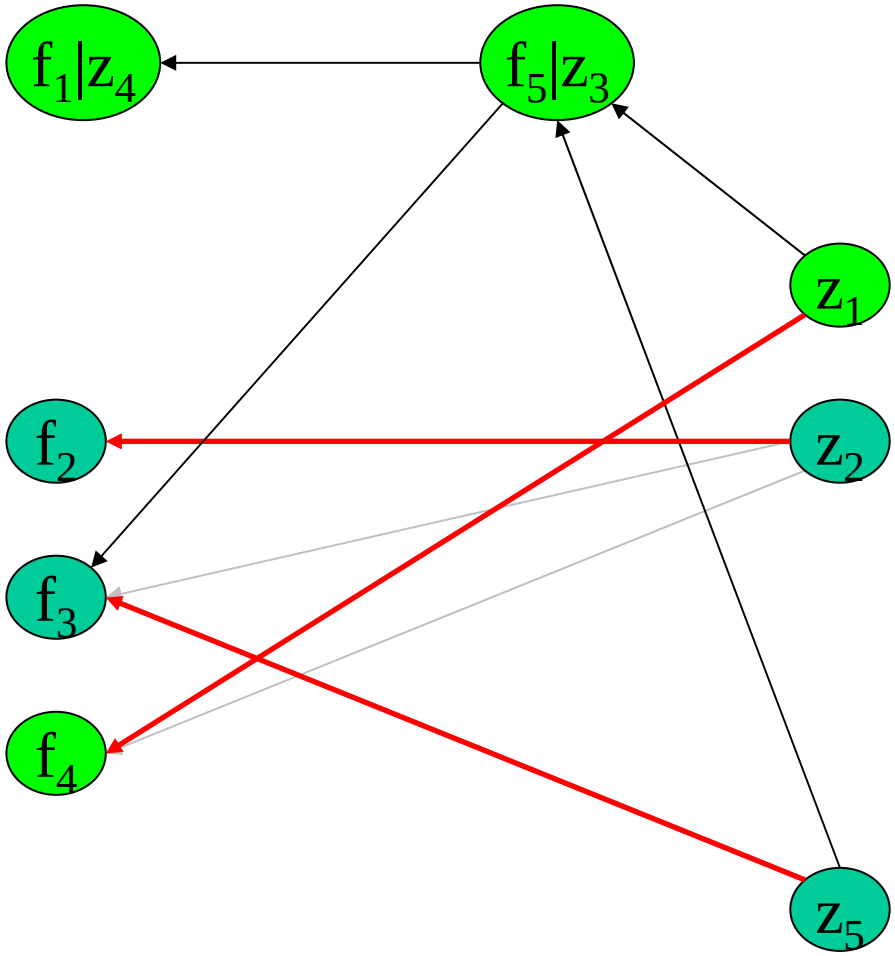
Construct a Directed Graph



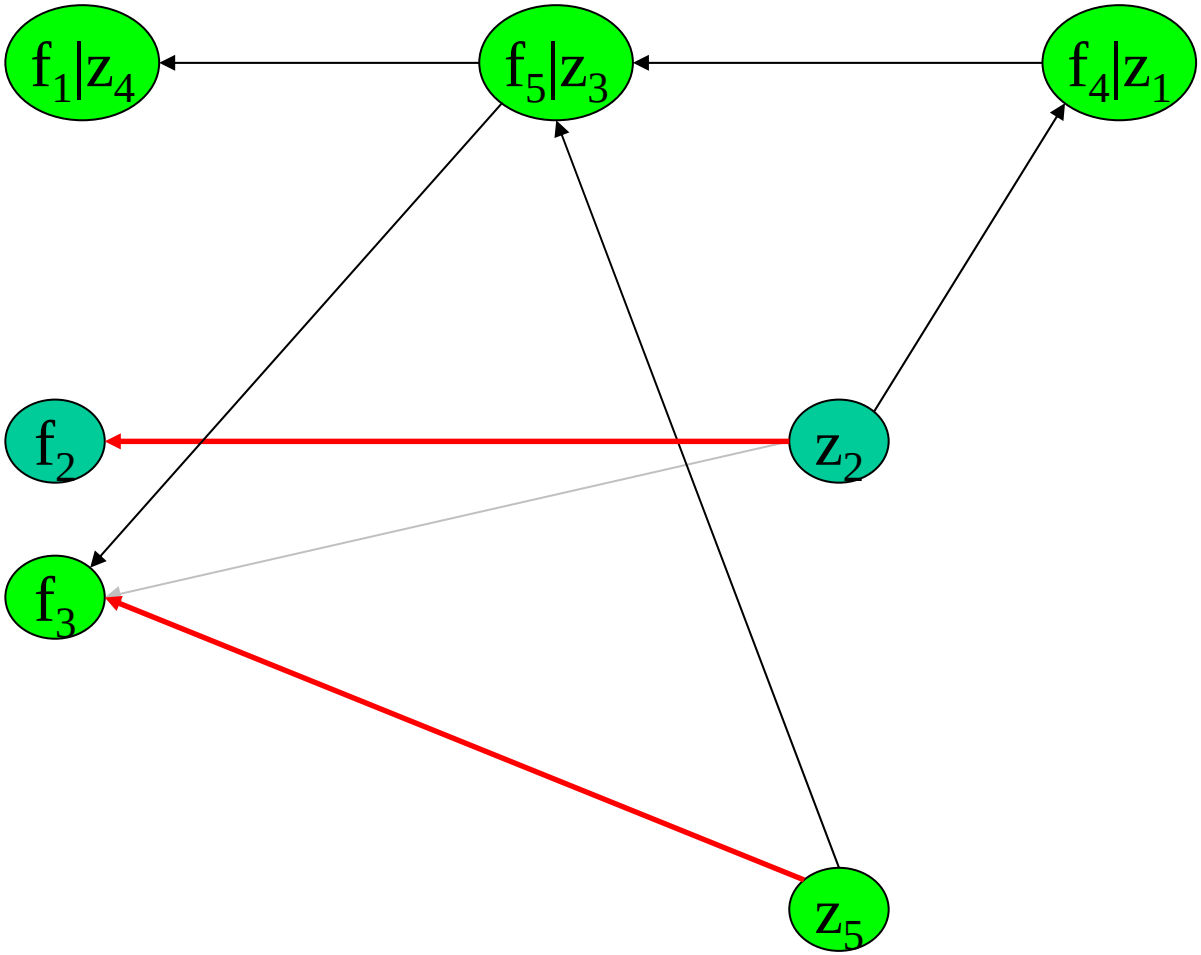
Construct a Directed Graph



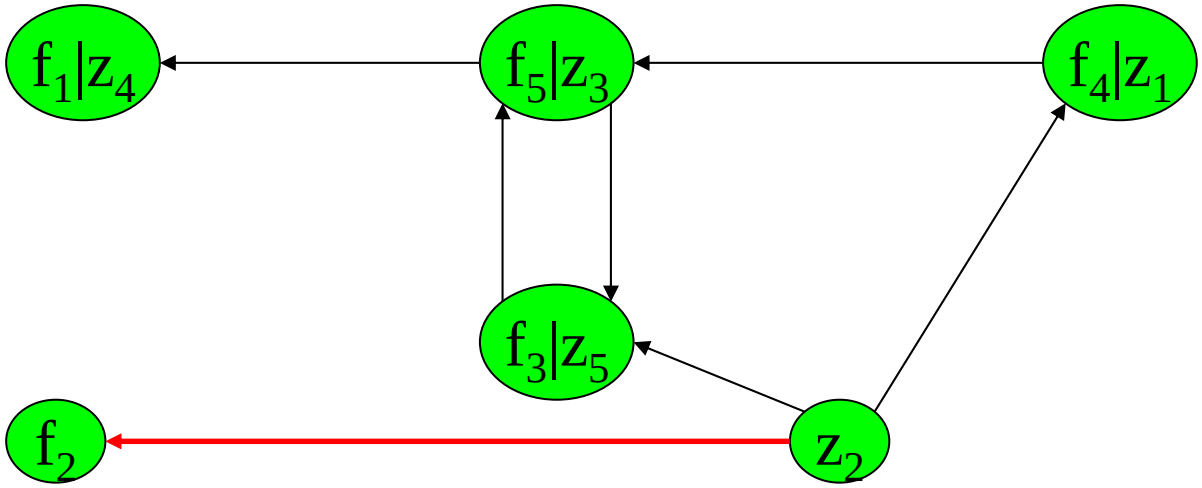
Construct a Directed Graph



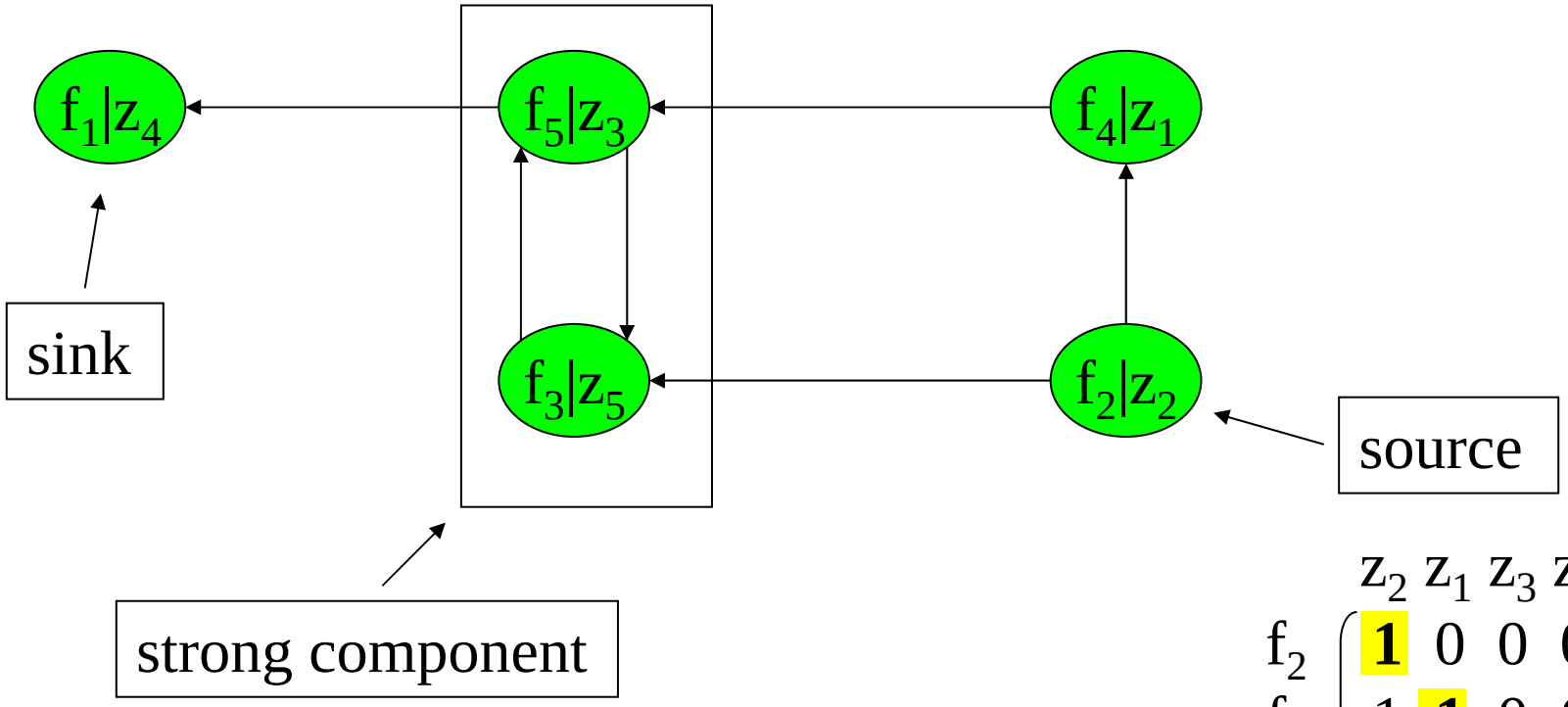
Construct a Directed Graph



Construct a Directed Graph



Construct a Directed Graph



$$\begin{array}{c} \\ f_2 \\ f_4 \\ f_3 \\ f_5 \\ f_1 \end{array} \begin{array}{c} \begin{array}{ccccc} z_2 & z_1 & z_3 & z_5 & z_4 \end{array} \\ \begin{pmatrix} \mathbf{1} & 0 & 0 & 0 & 0 \\ 1 & \mathbf{1} & 0 & 0 & 0 \\ 1 & 0 & \mathbf{1} & \mathbf{1} & 0 \\ 0 & 1 & \mathbf{1} & \mathbf{1} & 0 \\ 0 & 0 & 1 & 0 & \mathbf{1} \end{pmatrix} \end{array}$$

⟹ Tarjan's algorithm

Transformation Algorithms and the BLT-Form (Block-Lower-Triangle Form)

Example of a regular DAE:

$$
\begin{aligned}
f_1(z_3,z_4) &= 0\\
f_2(z_2) &= 0\\
f_3(z_2,z_3,z_5) &= 0\\
f_4(z_1,z_2) &= 0\\
f_5(z_1,z_3,z_5) &= 0
\end{aligned}
\qquad
\begin{aligned}
f_1(z_3,[z_4]) &= 0\\
f_2([z_2]) &= 0\\
f_3(z_2,z_3,[z_5]) &= 0\\
f_4([z_1],z_2) &= 0\\
f_5(z_1,[z_3],z_5) &= 0
\end{aligned}
\qquad
\begin{aligned}
f_2(\underline{z_2}) &= 0\\
f_4(\underline{z_1},z_2) &= 0\\
f_3(z_2,\underline{z_3},\underline{z_5}) &= 0\\
f_5(z_1,\underline{z_3},\underline{z_5}) &= 0\\
f_1(z_3,\underline{z_4}) &= 0
\end{aligned}
$$

BLT-form of the adjacence matrix

$$
\begin{array}{c} \\ f_1 \\ f_2 \\ f_3 \\ f_4 \\ f_5 \end{array}
\begin{array}{c}
\begin{array}{ccccc} z_1 & z_2 & z_3 & z_4 & z_5 \end{array} \\
\begin{pmatrix} 0 & 0 & 1 & 1 & 0 \\ 0 & 1 & 0 & 0 & 0 \\ 0 & 1 & 1 & 0 & 1 \\ 1 & 1 & 0 & 0 & 0 \\ 1 & 0 & 1 & 0 & 1 \end{pmatrix}
\end{array}
\qquad
\begin{array}{c} \\ f_1 \\ f_2 \\ f_3 \\ f_4 \\ f_5 \end{array}
\begin{array}{c}
\begin{array}{ccccc} z_1 & z_2 & z_3 & z_4 & z_5 \end{array} \\
\begin{pmatrix} 0 & 0 & 1 & \mathbf{1} & 0 \\ 0 & \mathbf{1} & 0 & 0 & 0 \\ 0 & 1 & 1 & 0 & \mathbf{1} \\ \mathbf{1} & 1 & 0 & 0 & 0 \\ 1 & 0 & \mathbf{1} & 0 & 1 \end{pmatrix}
\end{array}
\qquad
\begin{array}{c} \\ f_2 \\ f_4 \\ f_3 \\ f_5 \\ f_1 \end{array}
\begin{array}{c}
\begin{array}{ccccc} z_2 & z_1 & z_3 & z_5 & z_4 \end{array} \\
\begin{pmatrix} \mathbf{1} & 0 & 0 & 0 & 0 \\ 1 & \mathbf{1} & 0 & 0 & 0 \\ 1 & 0 & \mathbf{1} & \mathbf{1} & 0 \\ 0 & 1 & \mathbf{1} & \mathbf{1} & 0 \\ 0 & 0 & 1 & 0 & \mathbf{1} \end{pmatrix}
\end{array}
$$

Structural Regularity of the Adjacence Matrix

- Transformation algorithm works on the model structure
  - Assign each variable to exact one equation (matching problem)
  - Find equations which have to be solved simultaneously

- Nevertheless, certain parameter settings could make a model singular

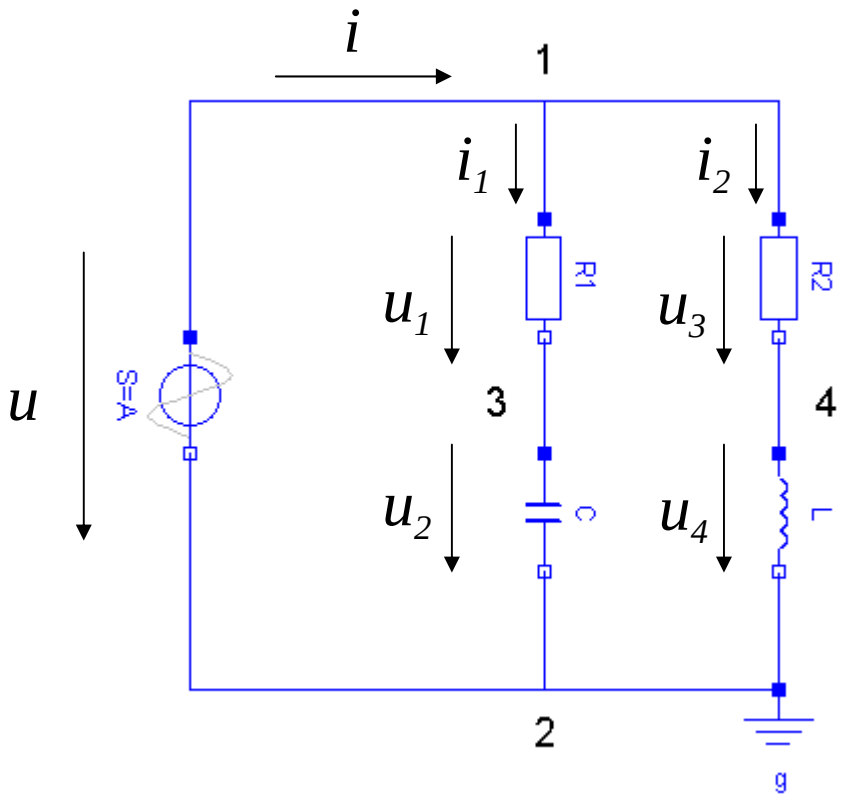
model singular

$$\Leftrightarrow \begin{vmatrix} a & b \\ 1 & 1 \end{vmatrix} = a - b = 0$$

$$\Leftrightarrow a = b$$

```
model SingularModel
  parameter Real a=2;
  parameter Real b=1;
  Real x,y;
equation
  a*der(x) + b*der(y) = sin(time);
  der(x) + der(y) = cos(time);
end SingularModel
```

Example: A Simple Electrical System



$$\boxed{u} = A \cdot \sin(\omega\, t)$$

$$u = \boxed{u_1} + \boxed{u_2}$$

$$\boxed{u_3} = R_2\, \boxed{i_2}$$

$$u = u_3 + \boxed{u_4}$$

$$u_1 = R_1\, \boxed{i_1}$$

$$\boxed{i} = i_1 + i_2$$

$$C \frac{\boxed{du_2}}{dt} = i_1$$

$$L \frac{\boxed{di_2}}{dt} = u_4$$

Efficiency Issues and Non-Linear Equations

- Transformed equation system
  - Efficient calculation of the unknowns and derivatives of the states
  - Solve single linear equations based on causality
- Algebraic loops
  - Linear equation systems can be treated by direct or iterative routines
  - Non-linear equation systems need more sophisticated solution techniques (only local convergence!)
- Real-time aspects
  - Causality of non-linear equation may influence the runtime efficiency

$$\underline{0} = \underline{f}\left(t, \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

$$\downarrow$$

$$\underline{0} = \underline{f}\left(t, \underline{z}(t), \underline{x}(t), \underline{u}(t), \underline{p}\right), \quad \underline{z}(t) = \begin{pmatrix} \underline{\dot{x}}(t) \\ \underline{y}(t) \end{pmatrix}$$

$$\downarrow$$

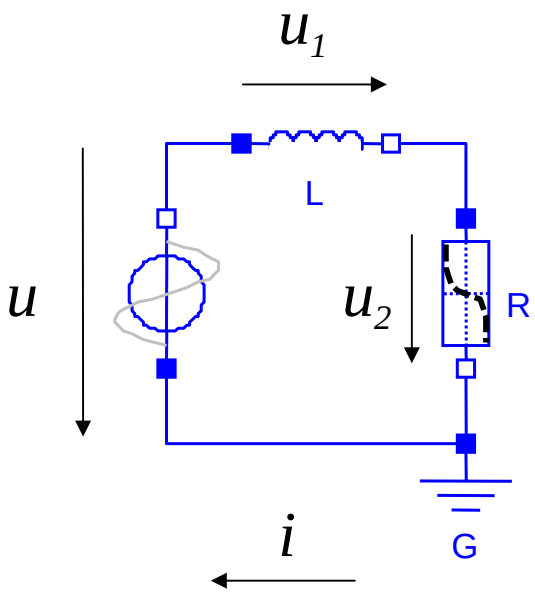
$$\underline{z}(t) = \begin{pmatrix} \underline{\dot{x}}(t) \\ \underline{y}(t) \end{pmatrix} = \underline{g}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

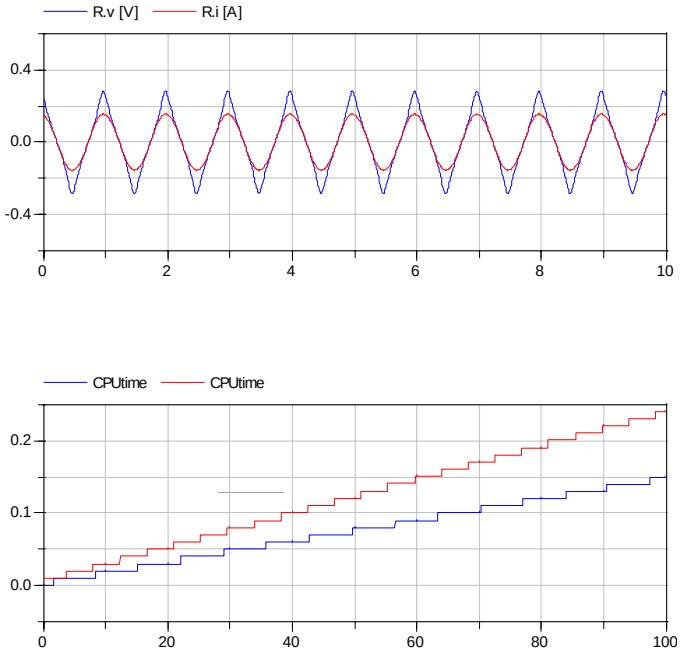
$$\downarrow$$

$$\underline{\dot{x}}(t) = \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\underline{y}(t) = \underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

Example: A Non-Linear Electrical System





$$u = A \cdot \sin(\omega\, t)$$

$$i = a \tanh\left(b\, u_2\right)$$

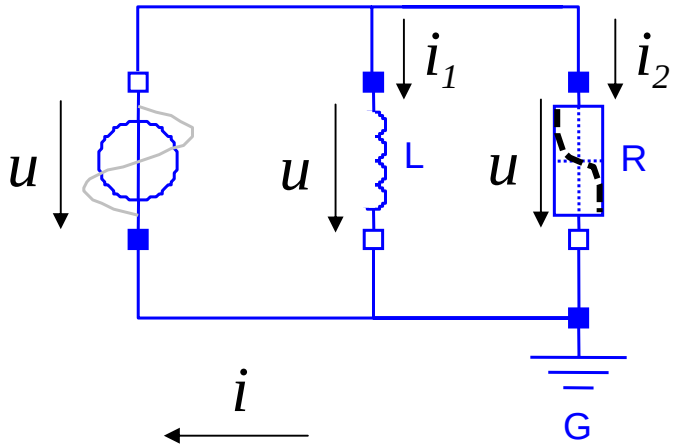
$$u = u_1 + u_2$$

$$L \frac{di}{dt} = u_1$$

Re-writing the non-linear equation (Causality):

$$u_2 = \frac{1}{2b} \log\left(\left(1 + i/a\right) \Big/ \left(1 - i/a\right) \right)$$

Example: A Non-Linear Electrical System



$$u = A \cdot \sin(\omega\, t)$$

$$i_1 = a \tanh\left(b\, u\right)$$

$$L \frac{di_2}{dt} = u$$

$$i = i_1 + i_2$$

Causality of the non-linear equation correct

Higher Index Problems
Structurally Singular Systems

- Higher-index DAEs
  - Differential index of a DAE
  - Structural singularity of the adjacence matrix
  - Index reduction method using symbolic differentiation of equations
- Numerical issues
  - Consistent initialization
  - Drift phenomenon
  - Dummy derivative method
- State selection mechanism in Modelica
  - See also initialization of 3-phase electrical system

$$\underline{0} = \underline{f}\left(t, \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

$$\downarrow$$

$$\underline{0} = \underline{f}\left(t, \underline{z}(t), \underline{x}(t), \underline{u}(t), \underline{p}\right), \quad \underline{z}(t) = \begin{pmatrix} \underline{\dot{x}}(t) \\ \underline{y}(t) \end{pmatrix}$$

$$\downarrow$$

$$\underline{z}(t) = \begin{pmatrix} \underline{\dot{x}}(t) \\ \underline{y}(t) \end{pmatrix} = \underline{g}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\downarrow$$

$$\underline{\dot{x}}(t) = \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\underline{y}(t) = \underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

Higher-Index-DAEs

General representation of DAEs:

$$\underline{0} = \underline{f}\left(t,\ \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

t	time
$\underline{\dot{x}}(t)$	vector of differentiated state variables
$\underline{x}(t)$	vector of state variables
$\underline{y}(t)$	vector of algebraic variables
$\underline{u}(t)$	vector of input variables
$\underline{p}$	vector of parameters and/or constants

Differential index of a DAE:

The minimal number of analytical differentiations of the equation system necessary to extract by algebraic manipulations an explicit ODE for all unknowns.

Higher-Index-DAEs

DAE with differential index 0:

$$\underline{0} = \underline{f}\left(t,\ \underline{\dot{x}}(t), \underline{x}(t), \underline{u}(t), \underline{p}\right) \longrightarrow \underline{\dot{x}}(t) = \underline{g}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

DAE with differential index 1:

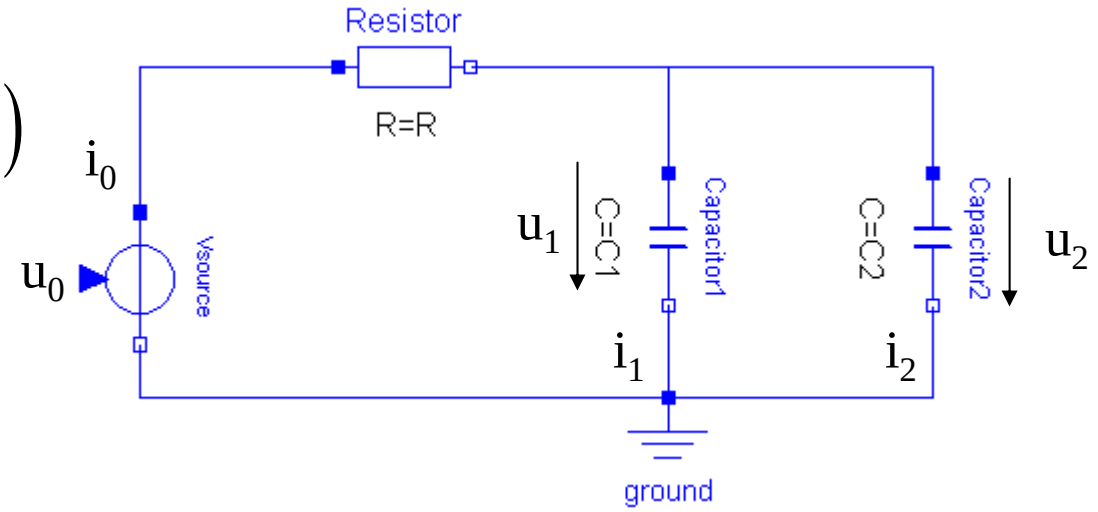
$$\underline{0} = \underline{f}\left(t,\ \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

$$\downarrow$$

$$\begin{aligned} \underline{\dot{x}}(t) &= \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right) \\ \underline{y}(t) &= \underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right) \end{aligned} \longrightarrow \begin{aligned} \underline{\dot{x}}(t) &= \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right) \\ \underline{\dot{y}}(t) &= \frac{d}{dt}\underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right) \end{aligned}$$

Higher-Index-DAE Example (index 2)

$$\underline{0} = \underline{f}\left(t,\ \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$



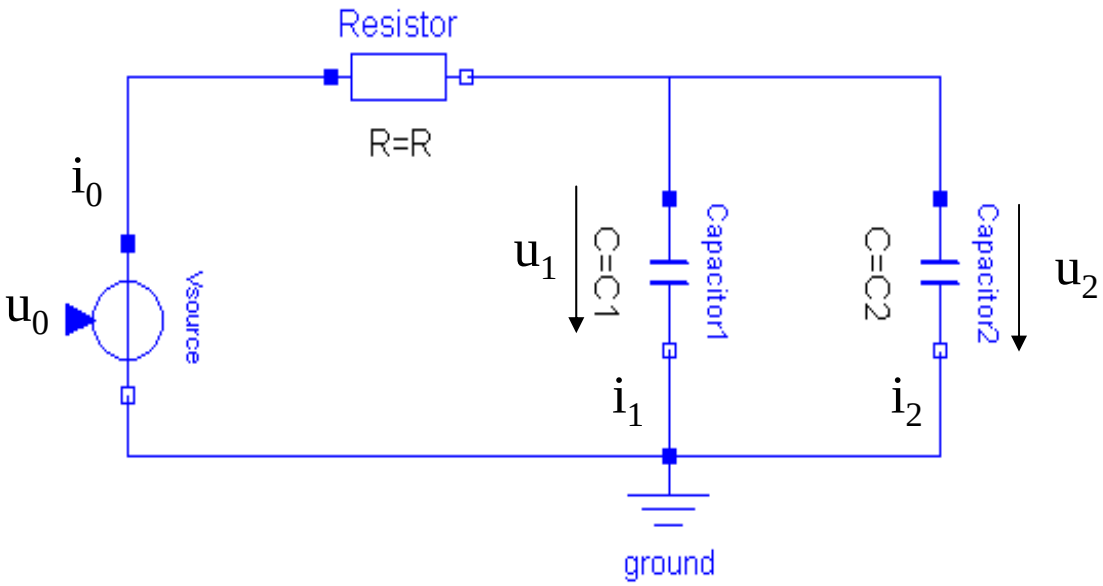
$$C_1 \cdot \dot{u}_1 = i_1$$
$$C_2 \cdot \dot{u}_2 = i_2$$
$$u_1 = u_2$$
$$i_0 = i_1 + i_2$$
$$u_0 = R \cdot i_0 + u_1$$

$$\mathbf{x} = \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} \quad \mathbf{y} = \begin{bmatrix} i_0 \\ i_1 \\ i_2 \end{bmatrix} \quad \mathbf{z} = \begin{bmatrix} \dot{u}_1 \\ \dot{u}_2 \\ i_0 \\ i_1 \\ i_2 \end{bmatrix}$$

5 equations and 5 unknowns.
BUT: system is singular!

constrained equation between states

Higher-Index-DAE Example (index 2)



$$C_1 \cdot \dot{u}_1 = i_1$$

$$C_2 \cdot \dot{u}_2 = i_2$$

~~$u_1 = u_2$~~

$$i_0 = i_1 + i_2$$

$$u_0 = R \cdot i_0 + u_1$$

$$\dot{u}_1 = \dot{u}_2$$

Algorithmic steps

- Differentiation of constrained equations
- Extracting underlying ODE (DAE of index 1)

$$\mathbf{x} = \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} \qquad \mathbf{z} = \begin{bmatrix} \dot{u}_1 \\ \dot{u}_2 \\ i_0 \\ i_1 \\ i_2 \end{bmatrix}$$

$$\mathbf{y} = \begin{bmatrix} i_0 \\ i_1 \\ i_2 \end{bmatrix}$$

$\Longrightarrow$ ODE with 5 equations and 5 unknowns

- Consistent initialization necessary

Higher-Index-DAEs -- Numerical Problems

- Consistent initial conditions
  - Relation between states are eliminated when differentiating
  - Initial conditions need to be determined using the algebraic constrains
  - Automatic procedure possible using assign algorithm on the constrained equations
- Drift phenomenon
  - Algebraic constrained no longer fulfilled during simulation
  - Even worse when simulating stiff problems

=> Dummy-Derivative method

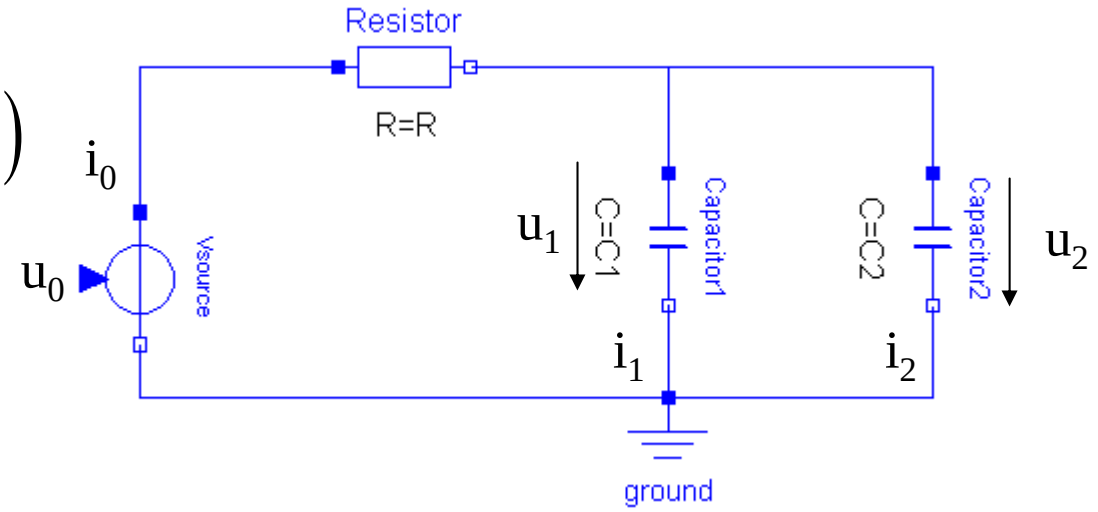
Principles of the Dummy-Derivative Method

- Matching algorithm fails
  - System is structurally singular
  - Find minimal subset of equations
    - more equations than unknown variables
  - Singularity is due to equations constraining states

- Differentiate subset of equations
  - Static state selection during compile time
    - choose one state and corresponding derivative as purely algebraic variable
      - so-called dummy-state and dummy derivative
    - by differentiation introduced variables are algebraic
    - continue matching algorithm
    - check initial conditions
  - Dynamic state selection during simulation time
    - store information on constrained states
    - make selection dynamically based on heuristic criteria
    - new state selection triggers an event (re-initialize states)

Dummy-Derivative method
Example (index 2)

$$\underline{0} = \underline{f}\left(t,\ \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

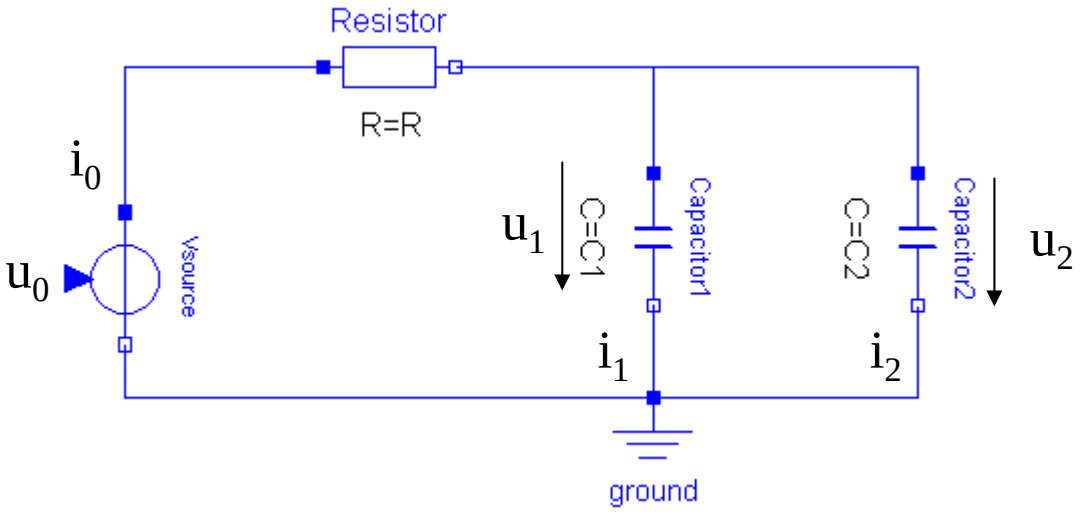


$$C_1 \cdot \dot{u}_1 = i_1$$
$$C_2 \cdot \dot{u}_2 = i_2$$
$$u_1 = u_2$$
$$i_0 = i_1 + i_2$$
$$u_0 = R \cdot i_0 + u_1$$

$$\mathbf{x} = \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} \quad \mathbf{y} = \begin{bmatrix} i_0 \\ i_1 \\ i_2 \end{bmatrix} \quad \mathbf{z} = \begin{bmatrix} \dot{u}_1 \\ \dot{u}_2 \\ i_0 \\ i_1 \\ i_2 \end{bmatrix}$$

constrained equation

Dummy-Derivative method
Example (index 2)



$$C_1 \cdot \dot{u}_1 = i_1$$
$$C_2 \cdot u_2' = i_2$$
$$u_1 = u_2$$
$$i_0 = i_1 + i_2$$
$$u_0 = R \cdot i_0 + u_1$$
$$\dot{u}_1 = u_2'$$

Algorithmic steps

- Differentiation of constrained equations
- Choose u_2 as dummy-state and u'_2 as dummy-derivative
- Extracting underlying ODE (DAE of index 1)

$$\mathbf{x} = \begin{bmatrix} u_1 \end{bmatrix}$$

$$\mathbf{y} = \begin{bmatrix} i_0 \\ i_1 \\ i_2 \\ u_2 \\ u_2' \end{bmatrix} \qquad \mathbf{z} = \begin{bmatrix} \dot{u}_1 \\ i_0 \\ i_1 \\ i_2 \\ u_2 \\ u_2' \end{bmatrix}$$

⟹ ODE with 6 equations and 6 unknowns

- Check initial condition

State Selection in Modelica

- Influence default state selection mechanism
  - Attribute `StateSelect stateSelect = StateSelect.default;`
  - Possible choices:

`never`	-	Do not use as state at all
`avoid`	-	Use as state, if it cannot be avoided (but only if variable appears differentiated and no other potential state with attribute default, prefer, or always can be selected)
`default`	-	Use as state if appropriate, but only if variable appears differentiated
`prefer`	-	Prefer it as state over those having the default value (also variables can be selected, which do not appear differentiated)
`always`	-	Do use it as a state

Initialization of Dynamic Models

- Initialization of “free” state variables
  - Transformed DAE after index-reduction
  - States can be chosen at start time
    - same number of additional equations and “free” states
- Initialization of parameters
  - Determine parameter settings
  - Parameters can be calculated at start time
    - same number of additional equations and “free” parameters
- Initialization mechanism in Modelica
  - attribute start
  - initial equation section
    - attribute fixed for parameters

$$\underline{0} = \underline{f}\left(t, \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

$$\downarrow$$

$$\underline{0} = \underline{f}\left(t, \underline{z}(t), \underline{x}(t), \underline{u}(t), \underline{p}\right), \quad \underline{z}(t) = \begin{pmatrix} \underline{\dot{x}}(t) \\ \underline{y}(t) \end{pmatrix}$$

$$\downarrow$$

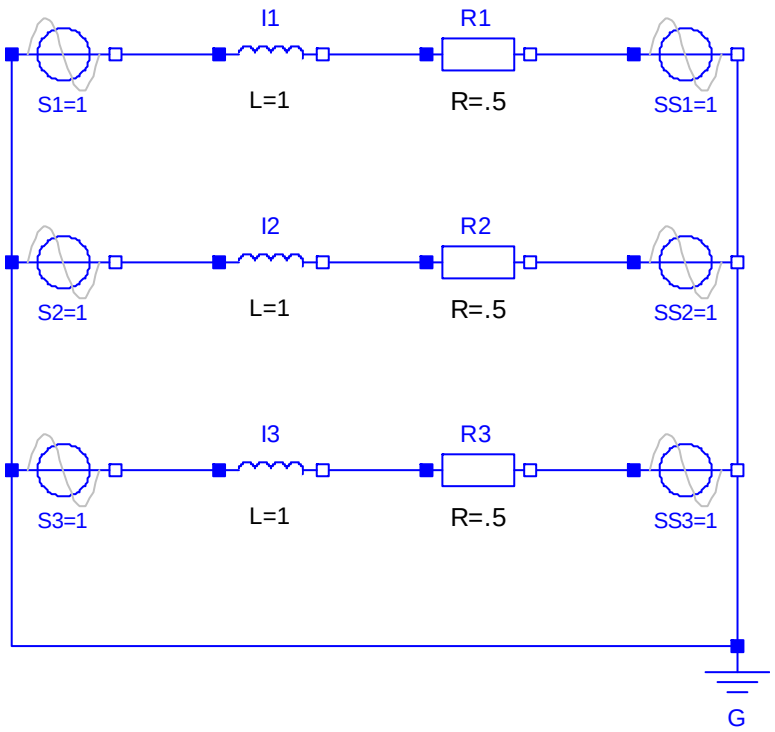
$$\underline{z}(t) = \begin{pmatrix} \underline{\dot{x}}(t) \\ \underline{y}(t) \end{pmatrix} = \underline{g}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

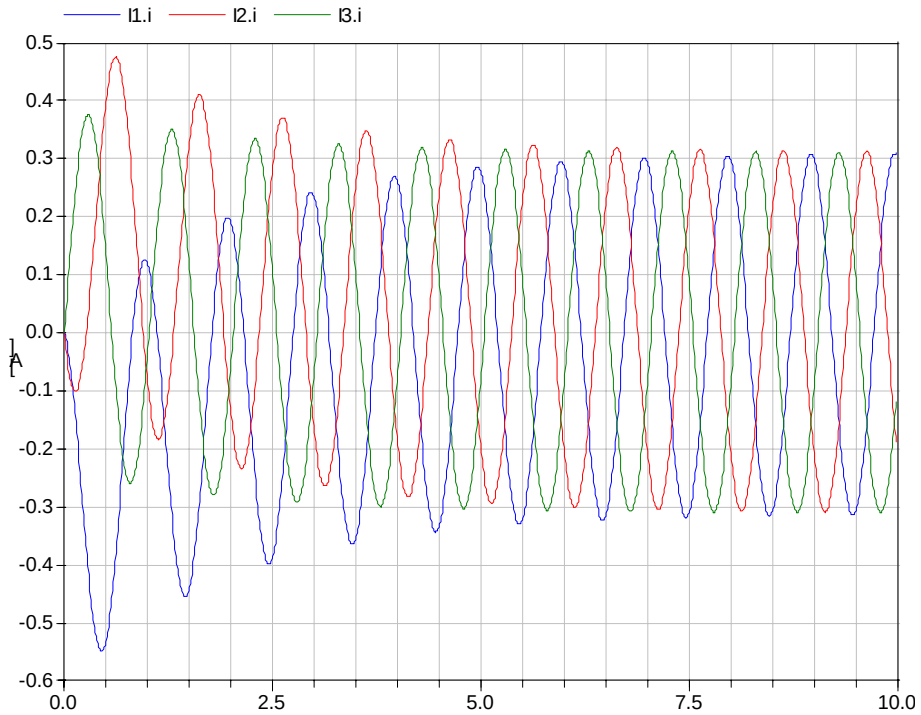
$$\downarrow$$

$$\underline{\dot{x}}(t) = \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\underline{y}(t) = \underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

Example: 3-Phase Electrical System





Steady-state initialization?

- States `I1.i, I2.i, I3.i` are not constant at initial time!
- Here: Initial values set to 0 (standard settings, attribute `start`)
- Transformation to rotating reference system necessary

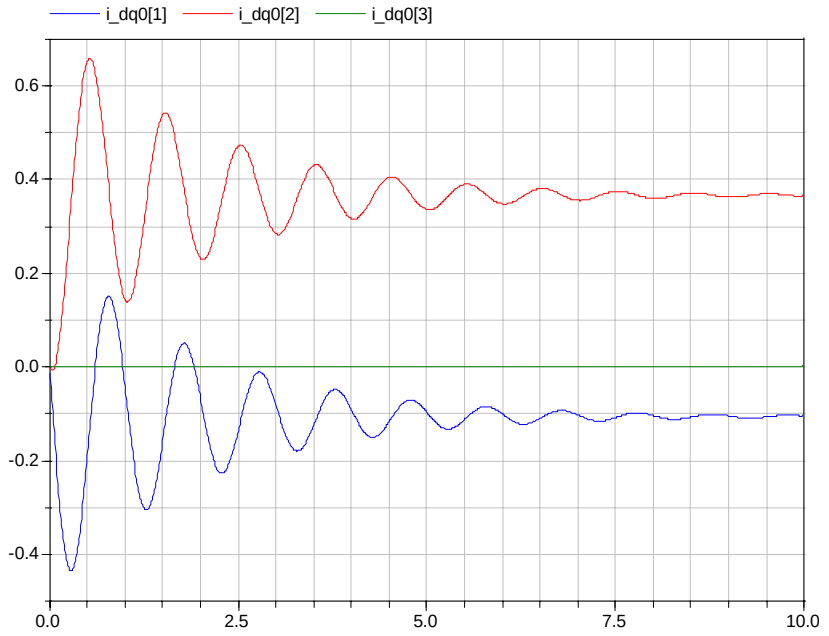
Example: 3-Phase Electrical System

Park-Transformation to rotating reference system:

- Write states as vector `i_abc[3] = {I1.i, I2.i, I3.i}`
- Park-transformation to dq0-reference frame

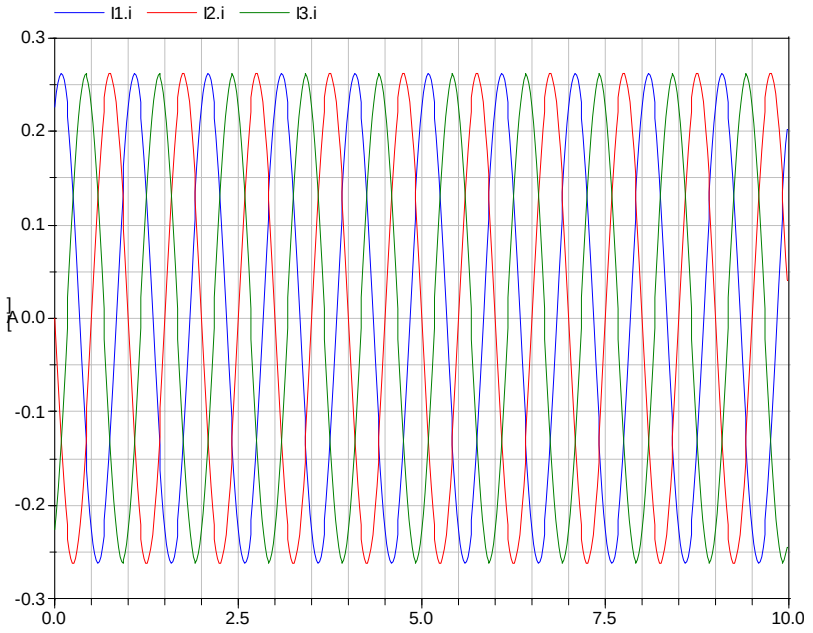
$$P = \frac{\sqrt{2}}{\sqrt{3}} \begin{pmatrix} \sin(\omega t) & \sin\left(\omega t + \frac{2\pi}{3}\right) & \sin\left(\omega t + \frac{4\pi}{3}\right) \\ \cos(\omega t) & \cos\left(\omega t + \frac{2\pi}{3}\right) & \cos\left(\omega t + \frac{4\pi}{3}\right) \\ 1/\sqrt{2} & 1/\sqrt{2} & 1/\sqrt{2} \end{pmatrix}$$

$$i\_dq0 = P \cdot i\_abc$$



Example: 3-Phase Electrical System Initialize States

```
model Test3PhaseSystem
  parameter Real shift=0.4;
  Real i_abc[3]={I1.i,I2.i,I3.i};
  Real i_dq0[3];
  …
initial equation
  der(i_dq0)={0,0,0};
equation
  …
  i_dq0 = P*i_abc;
end Test3PhaseSystem
```

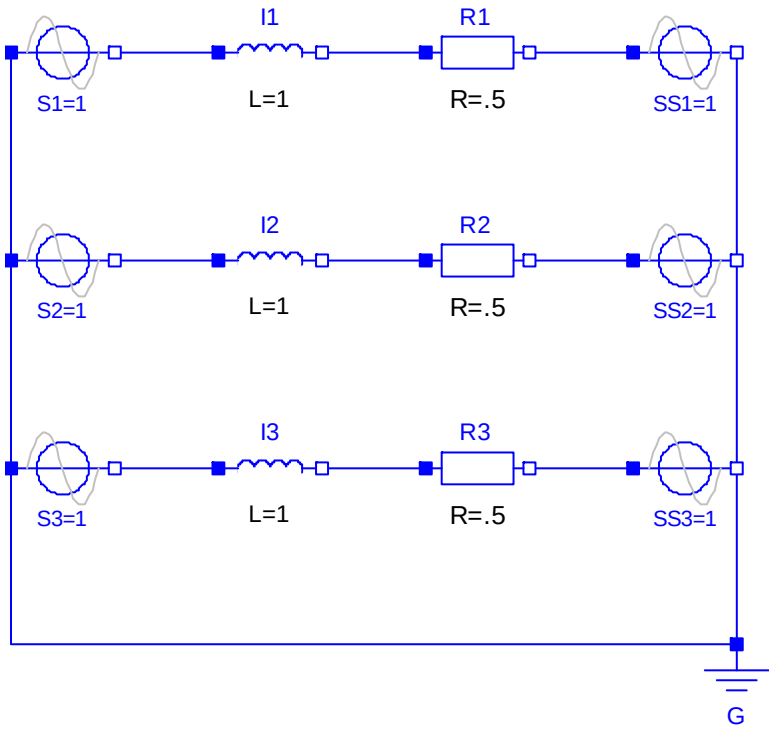


Steady-state initialization:

- Derivatives of `i_dq0` are only introduced during initialization
- Differentiation of `i_dq0 = P*i_abc` necessary
- No higher-index problem

Example: 3-Phase Electrical System Initialize Parameters

```
model Test3PhaseSystem
  parameter Real shift(fixed=false,start=0.1);
  Real i_abc[3]={I1.i,I2.i,I3.i}, u_abc[3]={S1.v,S2.v,S3.v};
  …
initial equation
  der(i_dq0)={0,0,0};
  power = -0.12865;
equation
  …
  u_dq0 = P*u_abc;
  i_dq0 = P*i_abc;
  power = u_dq0*i_dq0;
end Test3PhaseSystem
```

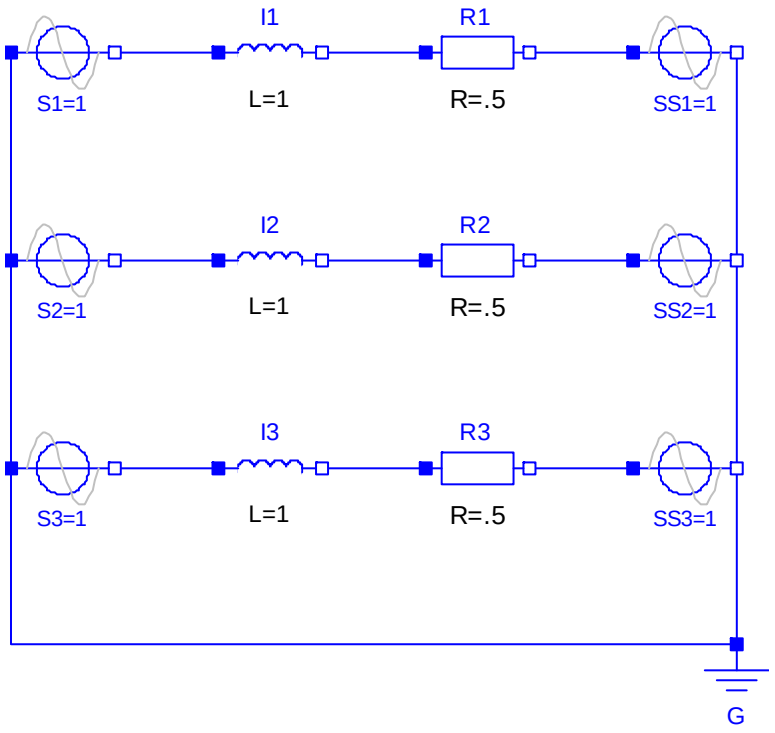


Parameter initialization:

- Non-linear equation, no unique solution
  `power=u_dq0*i_dq0=-0.12865`
- Attribute `fixed` (default `true`)
- Attribute `start` (default `0`)

Example: 3-Phase Electrical System Influence State Selection

```
model Test3PhaseSystem
  Real i_abc[3]={I1.i,I2.i,I3.i};
  Real i_dq0[3](each stateSelect=StateSelect.always);
  …
initial equation
  …
equation
  …
  i_dq0 = P*i_abc;
end Test3PhaseSystem
```



State selection:

- Introduce `i_dq0` as states

```
Real di_dq0[3];
der(i_dq0)=di_dq0;
```

- Constrained equation between states must be differentiated

```
i_dq0 = P*i_abc;
```

Example: 3-Phase Electrical System
Introduce Dummy-States/Derivatives

Mathematical formulas to the Park-transformation:
(using trigonometric identities)

$$P = \frac{\sqrt{2}}{\sqrt{3}} \begin{pmatrix} \sin(\omega t) & \sin\left(\omega t + \frac{2\pi}{3}\right) & \sin\left(\omega t + \frac{4\pi}{3}\right) \\ \cos(\omega t) & \cos\left(\omega t + \frac{2\pi}{3}\right) & \cos\left(\omega t + \frac{4\pi}{3}\right) \\ 1/\sqrt{2} & 1/\sqrt{2} & 1/\sqrt{2} \end{pmatrix}$$

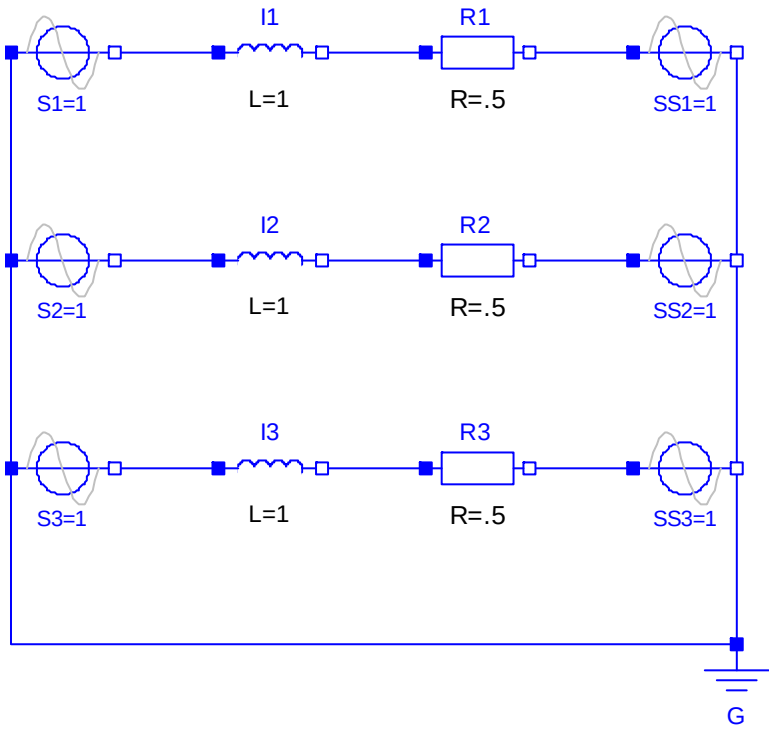
$$i\_dq0 = P \cdot i\_abc$$

$$P \cdot P^T = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \qquad P' \cdot P^T = \begin{pmatrix} 0 & \omega & 0 \\ -\omega & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\frac{d}{dt} i\_dq0 = \omega \cdot \begin{pmatrix} i\_dq0_2 \\ -i\_dq0_1 \\ 0 \end{pmatrix} + P \cdot \frac{d}{dt} i\_abc$$

Example: 3-Phase Electrical System Introduce Dummy-States/Derivatives

```
model Test3PhaseSystem
  Real i_abc[3]={I1.i,I2.i,I3.i};
  Real i_dq0[3];
  Real di_dq0[3]=2*pi*{i_dq0[2],-i_dq0[1],0} + P*der(i_abc);
  …
initial equation
  di_dq0={0,0,0};
equation
  …
  i_dq0 = P*i_abc;
end Test3PhaseSystem
```



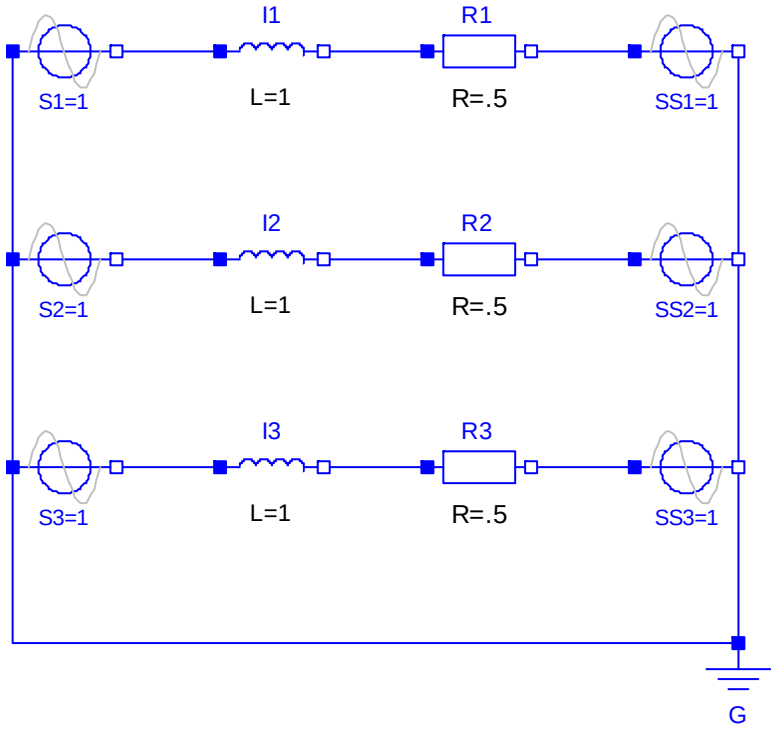
State selection:

- Introduce `di_dq0` as dummy derivative
- Only used during initialization
- No differentiation necessary
- States `I1.i, I2.i, I3.i` used during simulation

Example: 3-Phase Electrical System
Introduce Dummy-States/Derivatives

State selection:

- Introduce `di_abc` as dummy derivative
- Rewrite inductor equation: `L*di = v;`
- No differentiation necessary
- Efficiency increase during simulation (real-time aspect)




```
model Test3PhaseSystem
  Real i_abc[3]={I1.i,I2.i,I3.i};
  Real di_abc[3]={I1.di,I2.di,I3.di};
  Real i_dq0[3];
  …
initial equation
  der(i_dq0)={0,0,0};
equation
  …
  i_dq0 = P*i_abc;
  der(i_dq0)=2*pi*{i_dq0[2],-i_dq0[1],0} + P*di_abc;
end Test3PhaseSystem
```

Numerical Integration of ODEs/DAEs

- Integration methods for ODEs
  - Single-step methods
    - explicit and implicit Runge-Kutta formulas
    - fixed and variable step-size
      - Richardson-Extrapolation
      - embedded Runge-Kutta Formulas (Dopri5)
  - Multi-step methods
    - explicit and implicit schemes
      - Adams/Bashforth/Moulton formulas
      - BDF-formulas (i.e. DASSL)
    - start-up using single-step methods (events)
  - Event handling
    - stop simulation and restart integration
- Stability region and stiffness detection
  - Linearize the system
  - Determine eigenvalues

$$\underline{0} = \underline{f}\left(t, \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

$$\downarrow$$

$$\underline{0} = \underline{f}\left(t, \underline{z}(t), \underline{x}(t), \underline{u}(t), \underline{p}\right), \quad \underline{z}(t) = \begin{pmatrix} \underline{\dot{x}}(t) \\ \underline{y}(t) \end{pmatrix}$$

$$\downarrow$$

$$\underline{z}(t) = \begin{pmatrix} \underline{\dot{x}}(t) \\ \underline{y}(t) \end{pmatrix} = \underline{g}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\downarrow$$

$$\underline{\dot{x}}(t) = \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\underline{y}(t) = \underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

Stability Analysis of Runge-Kutta Methods

ODE problem:

$$\dot{\underline{x}}(t) = \underline{f}\left(t, \underline{x}(t)\right)$$

describing disturbance:

$$\underline{y}'(t) = J(t) \cdot \underline{y}(t), \quad J(t) = \frac{\partial \underline{f}}{\partial \underline{x}}(t, \underline{x})$$

Euler integration:
(J constant)

$$\underline{y}_{m+1} = \underline{y}_m + \Delta t \cdot J \cdot \underline{y}_m = R(\Delta t \cdot J) \cdot \underline{y}_m$$

$$R(z) = 1 + z$$

eigenvector $\underline{y}_0$
eigenvalue λ

$$\underline{y}_m = \left[R(\Delta t \cdot \lambda) \right]^m \cdot \underline{y}_0$$

bounded solution, iff

$$\left| R(\Delta t \cdot \lambda) \right| \leq 1, \quad \lambda \text{ eigenvalue of } J$$

Stability Analysis of Runge-Kutta Methods

Dahlquist test equation: $y' = \lambda \cdot y, \quad y_0 = 1, \quad z = \Delta t \cdot \lambda$

Stability function $R(z)$ is corresponding numerical solution at $t + \Delta t$:

Runge-Kutta method (order=p): $R(z) = 1 + \frac{z}{1!} + \ldots + \frac{z^p}{p!} + O(z^{p+1})$

Runge-Kutta method (order=s, explicit, s_stage): $R(z) = 1 + \frac{z}{1!} + \ldots + \frac{z^s}{s!}$

Dopri5 (order=5, explicit, 6_stage): $R(z) = 1 + \frac{z}{1!} + \ldots + \frac{z^5}{5!} + \frac{z^6}{600}$

bounded solution, iff $|R(\Delta t \cdot \lambda)| \leq 1, \quad \lambda$ eigenvalue of J

Stability Region for Explicit Runge-Kutta Methods

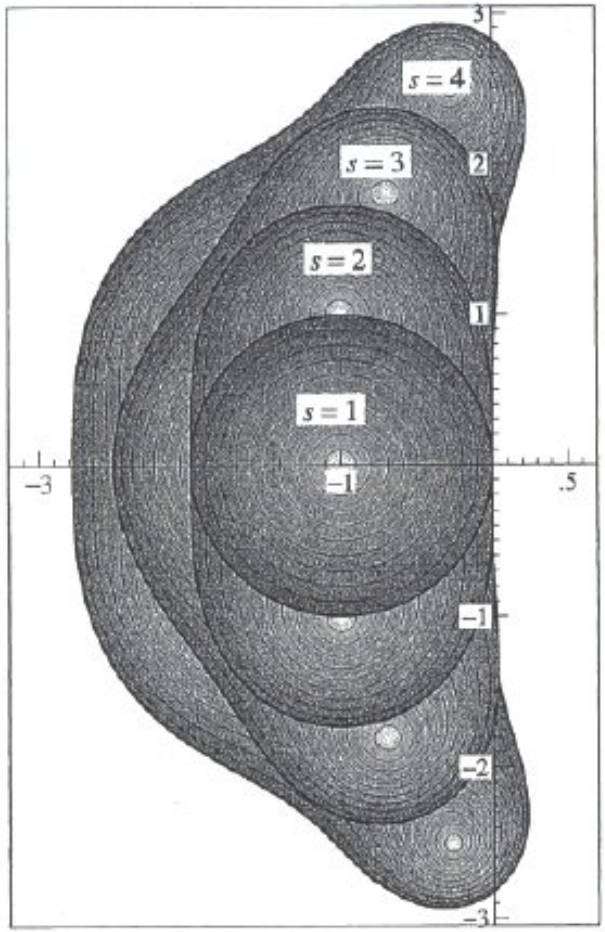


Fig. 2.1. Stability domains for explicit Runge-Kutta methods of order $p = s$

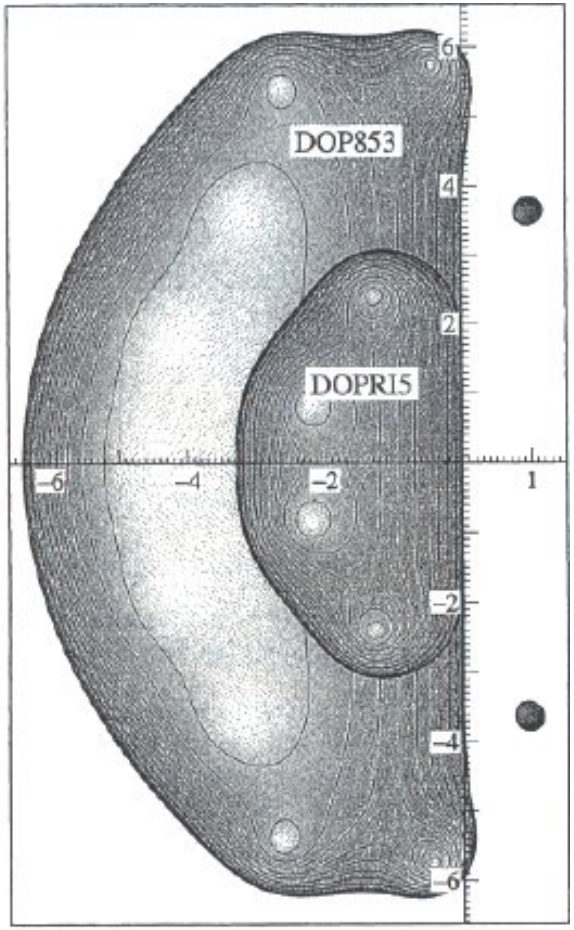


Fig. 2.2. Stability domains for DOPRI methods

Stability Region for Implicit Runge-Kutta Methods

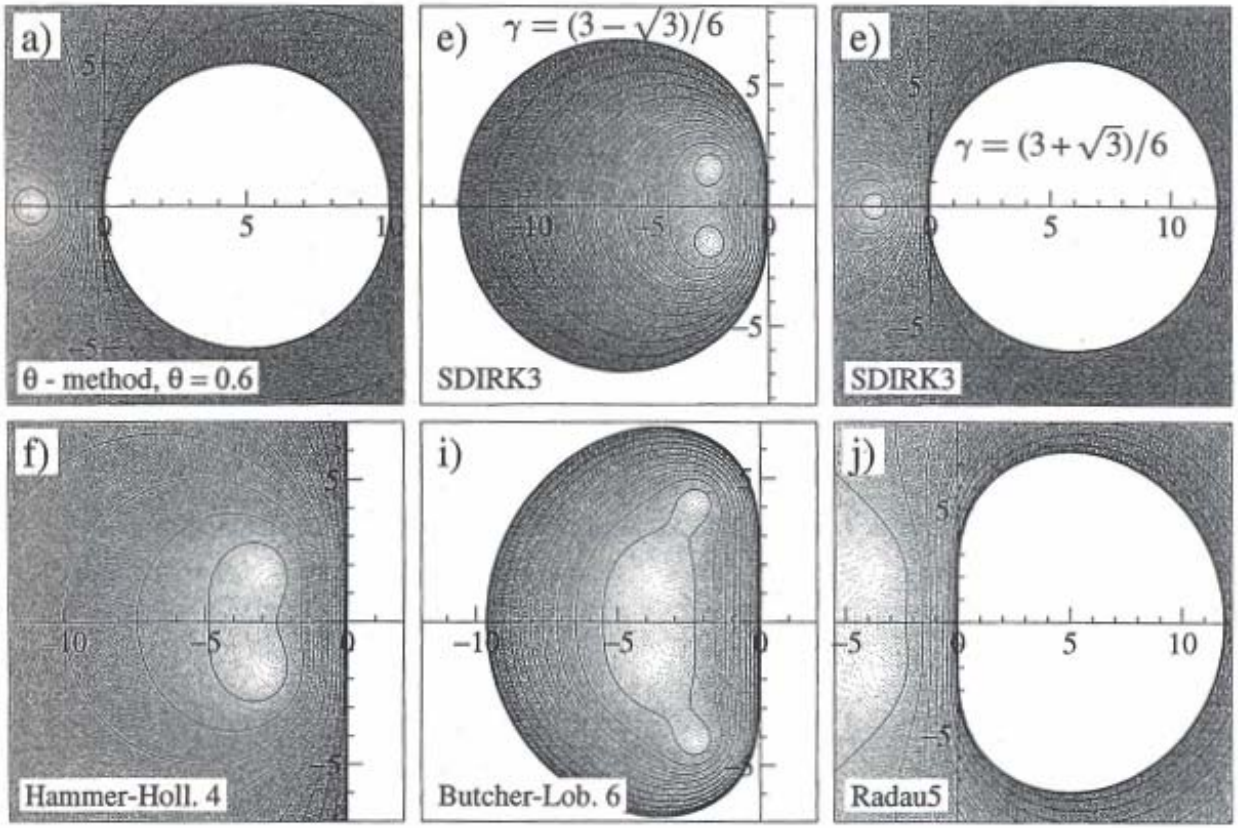


Fig. 3.1. Stability domains for implicit Runge-Kutta methods

Stability Region for Adams-Multi-Step Methods

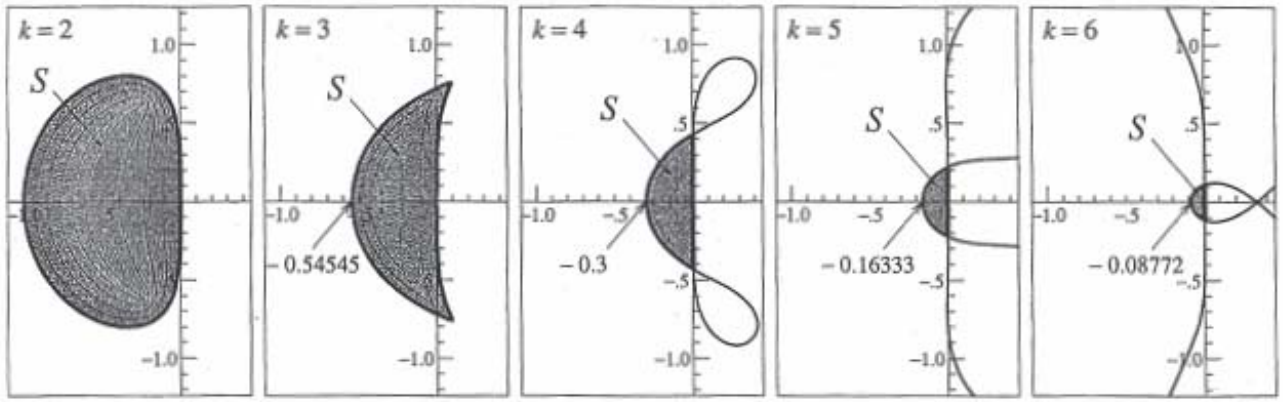


Fig. 1.2. Stability domains for explicit Adams methods

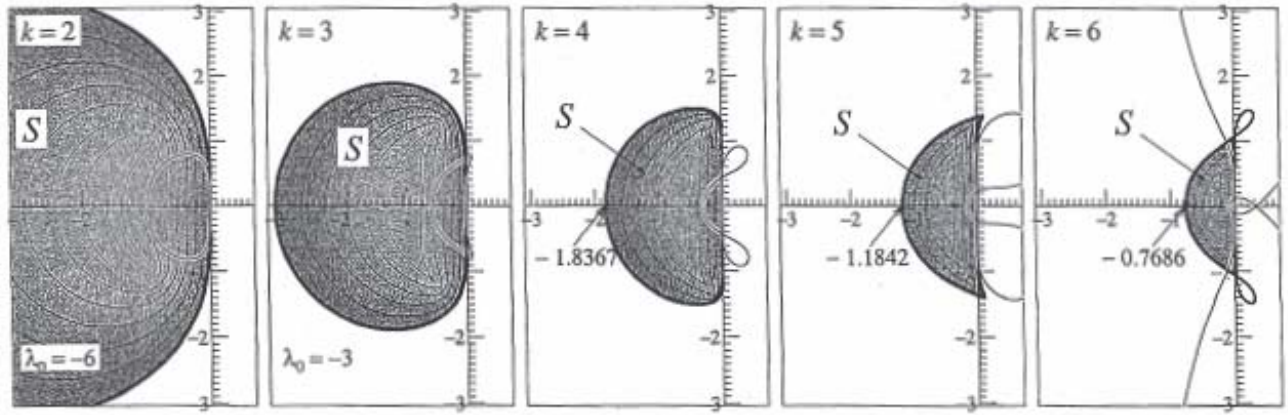


Fig. 1.3. Stability domains of implicit Adams methods, compared to those of the explicit ones

Stability Region for BDF – Methods (i.e. DASSL)

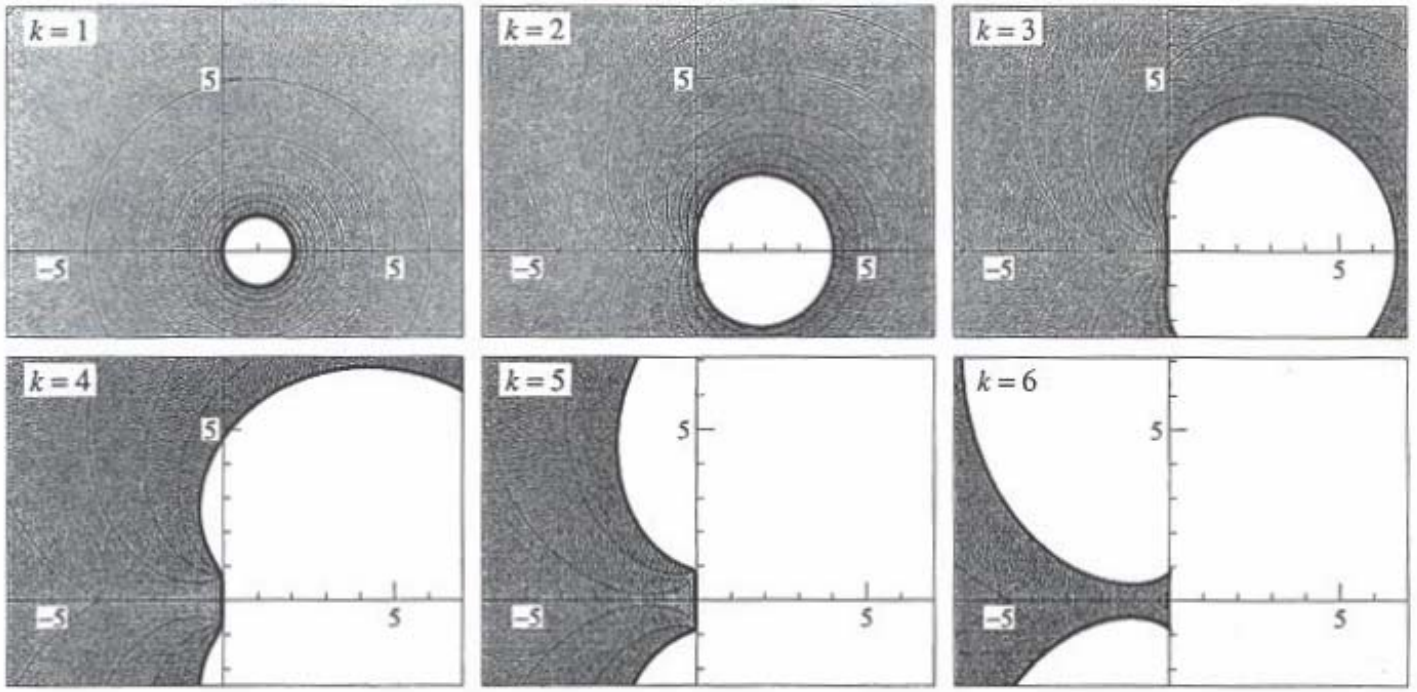


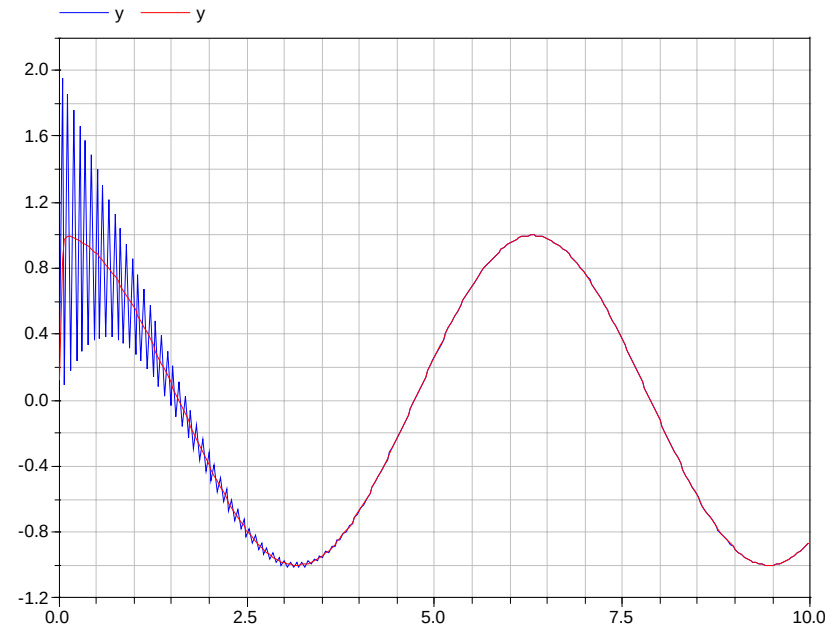
Fig. 1.6. Root locus curves and stability domains of BDF methods

Numerical Examples (Stability Region)

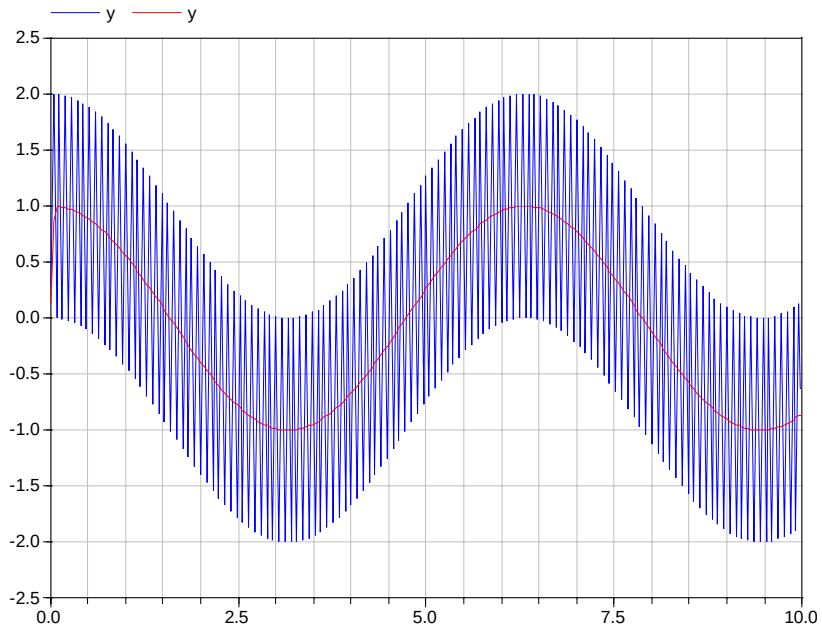
- Curtiss & Hirschfelder
  - Transition phase at the initial point
  - Determine maximal fixed step-size

$$y' = -50\left(y - \cos(t)\right), \quad \text{eigenvalue } \lambda = -50$$

$\Delta t = 0.039$: (explicit Euler)



$\Delta t = 0.04$: (explicit Euler)

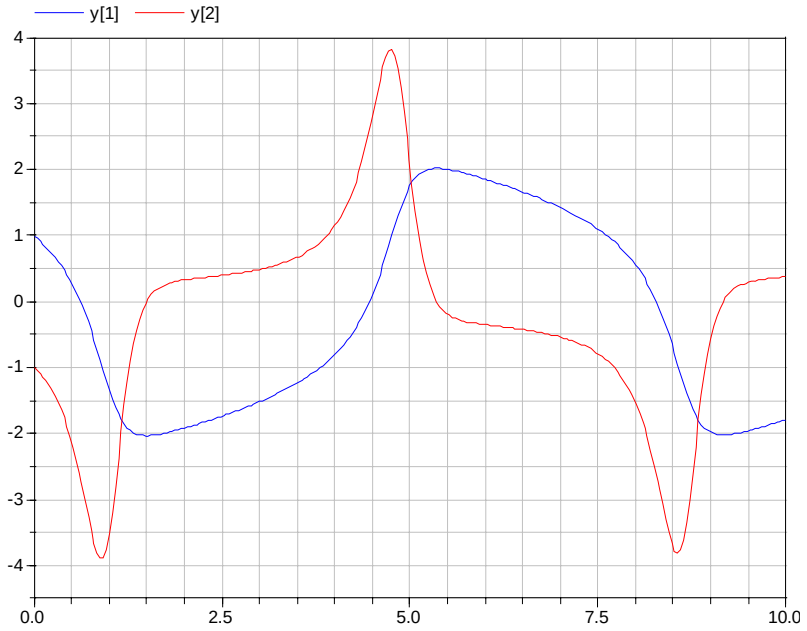


Numerical Examples (Stability Region and Stiffness)

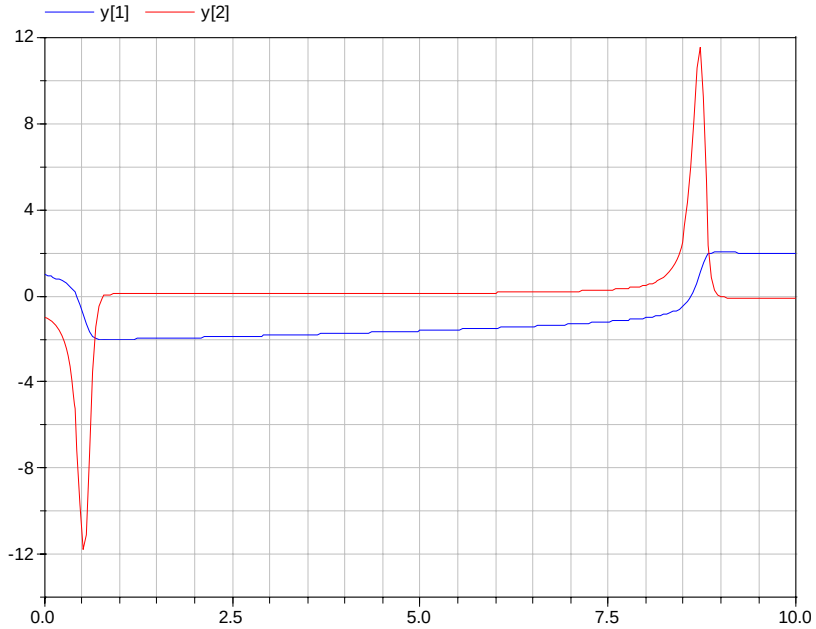
- Van der Pol
  - Simple nonlinear equation describing electrical systems
  - Stiff system, if $\varepsilon >> 1$.

$$y_1' = y_2$$
$$y_2' = \varepsilon\left(1 - y_1^2\right) y_2 - y_1 \qquad \text{mit } J(t) = \begin{pmatrix} 0 & 1 \\ -2\varepsilon y_1 y_2 - 1 & \varepsilon\left(1 - y_1^2\right) \end{pmatrix}$$

$\varepsilon = 2$:



$\varepsilon = 8$:



Determine Stability Region (Van der Pol equation)

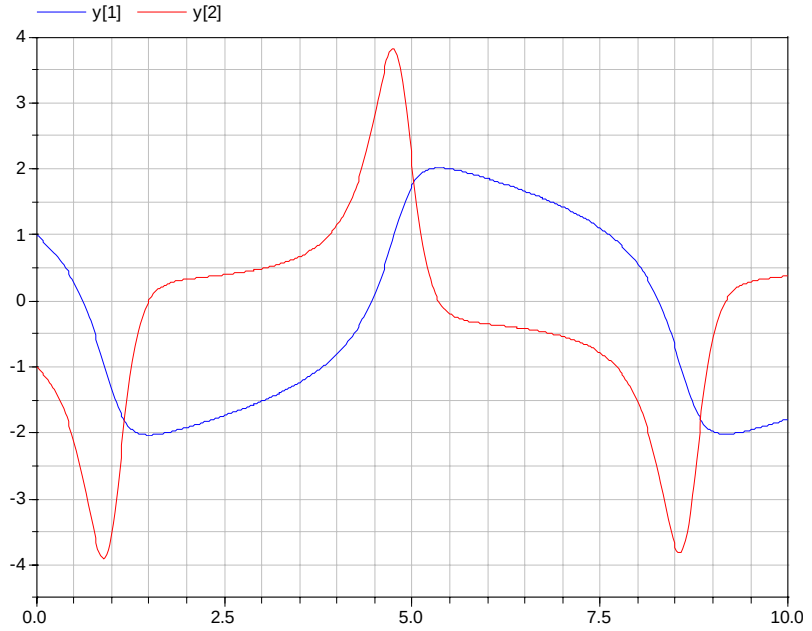
- Linearize the system at initial time
  - Calculate the Jacobians
  - Read matrix into Matlab
  - Determine the eigenvalues
  - Calculate maximal step-size

$$\dot{\underline{x}}(t) = \underline{h}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right) \qquad \underline{y}(t) = \underline{k}\left(t, \underline{x}(t), \underline{u}(t), \underline{p}\right)$$

$$\longrightarrow$$

$$\dot{\underline{x}}(t) = A\underline{x}(t) + B\underline{u}(t) \qquad \underline{y}(t) = C\underline{x}(t) + D\underline{u}(t)$$

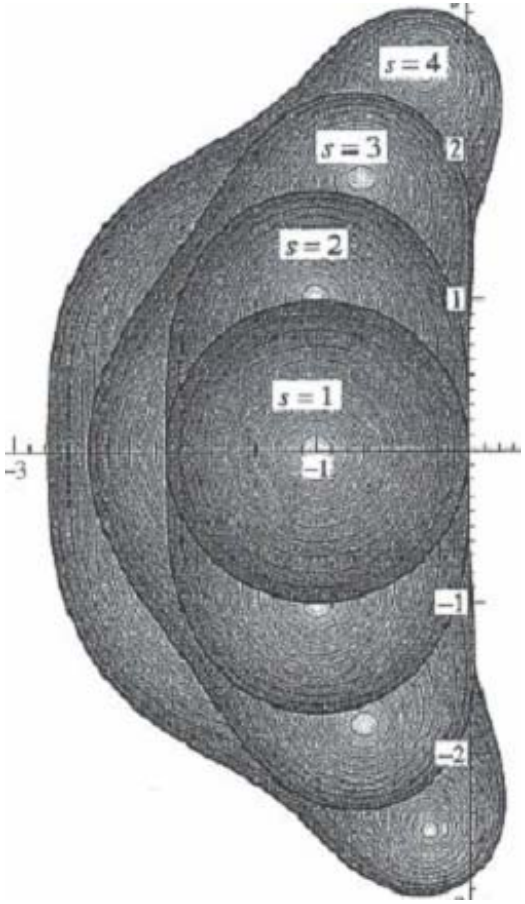
```
>> A = tloadlin
>c:\…\dslin.mat loaded.
A =         0    1.0000
    39.0000         0
>> l=eig(A)
l =  6.245
    -6.245

>>delta_t=2/6.245
delta_t = 0.3203
```



Determine Stability Region (Van der Pol equation)

bounded solution, iff

$$\left|R(\Delta t \cdot \lambda)\right| \le 1, \quad \lambda \text{ eigenvalue of } J$$



explicit Euler method: $R(z) = 1 + z$

$$\left|R(\Delta t \cdot \lambda)\right| = \left|1 + \Delta t \cdot \lambda\right| = \left|\begin{pmatrix}1\\0\end{pmatrix} + \Delta t \begin{pmatrix}x\\y\end{pmatrix}\right| \le 1$$

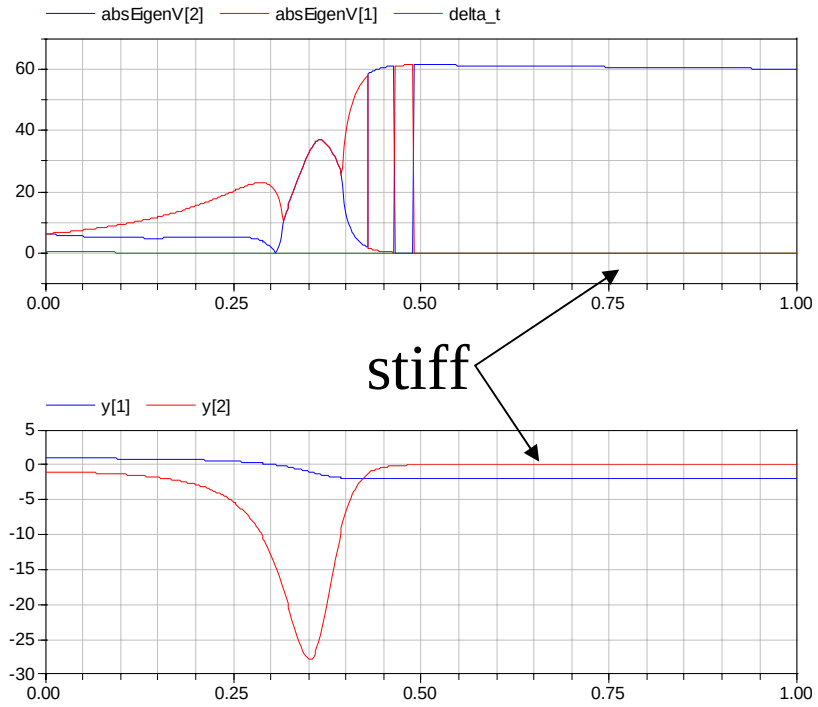
$$\Leftrightarrow (1 + \Delta t \cdot x)^2 + (\Delta t \cdot y)^2 \le 1$$

$$\Leftrightarrow \Delta t^2 (x^2 + y^2) + 2 \cdot \Delta t \cdot x \le 0$$

$$\Leftrightarrow \Delta t \le -\frac{2 \cdot x}{x^2 + y^2}$$

Determine Stability Region (Van der Pol equation)

- Calculate eigenvalues during simulation

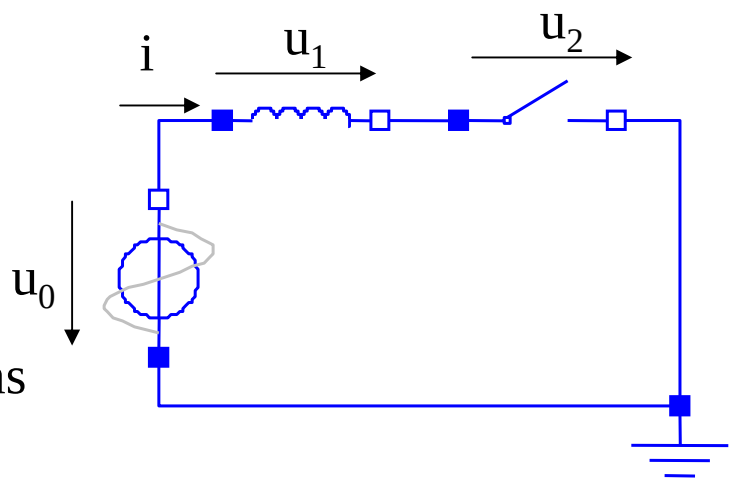



```
model VanDerPol
  import Matrices.eigenValues;
  import Vectors.norm;
  parameter Real epsilon=2;
  Real y[2] (start={1,-1});
  Real eigenV[2,2];
  Real delta_t;
equation
  der(y[1]) = y[2];
  der(y[2]) = epsilon*(1 - y[1]*y[1])*y[2] - y[1];
  eigenV=eigenValues(
           [                    0,                    1;
            -2*epsilon*y[1]*y[2]-1, epsilon*(1-y[1]*y[1])]);
  delta_t=max(-2*eigenV[1,1]/(eigenV[1,:]*eigenV[1,:]),
              -2*eigenV[2,1]/(eigenV[2,:]*eigenV[2,:]));
end VanDerPol;
```

$\Longrightarrow \quad \Delta t_{\max} = 0.0326524$

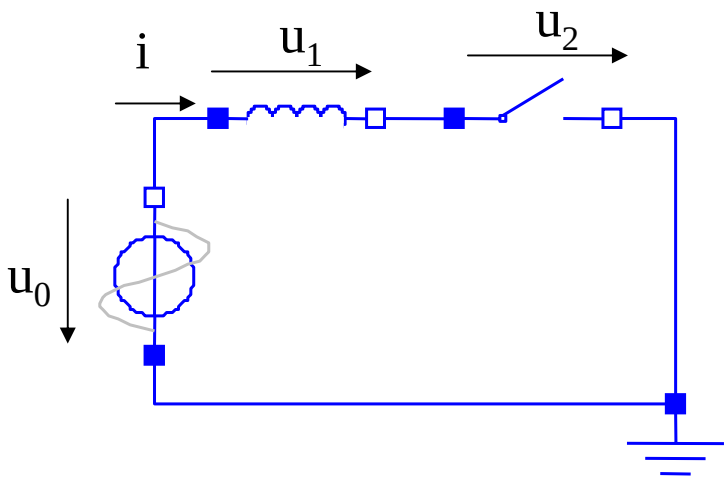
Event Handling
Motivation and Numerical Issues

- Need of discontinuous components
  - Detailed modeling too complex
  - Model parameters are not known for detailed models
  - Non-ideal approximation leads to stiff systems
  - Speed up simulation time (omit stiffness)



- Numerical problems at events
  - ODE solver based on polynomial approximation
  - Usually some signals are not continuous or differentiable
  - Fixed step size leads to bad approximation of events
  - Varying higher-index problems can occur at events

Example: Non-Ideal Switch Stiffness Problem



$$u_0 = A\sin(\omega t) \quad u_2 = Ri \quad L\frac{di}{dt} = u_1 \quad u_0 = u_1 + u_2$$

$$\longrightarrow \quad L\frac{di}{dt} = A\sin(\omega t) - R\,i \quad \downarrow \quad \boxed{\lambda = -\frac{R}{L}}$$

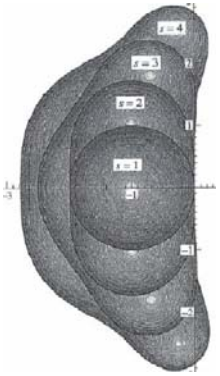
Non-ideal switch:

closed: $u_2 = R\,i, \quad R=1e\text{-}5$

open: $G\,i = u_2, \quad G=1e\text{-}5$

$$u_0 = A\sin(\omega t) \quad i = Gu_2 \quad L\frac{di}{dt} = u_1 \quad u_0 = u_1 + u_2$$

$$\longrightarrow \quad L\frac{di}{dt} = A\sin(\omega t) - \frac{i}{G} \quad \downarrow \quad \boxed{\lambda = -\frac{1}{L \cdot G}}$$

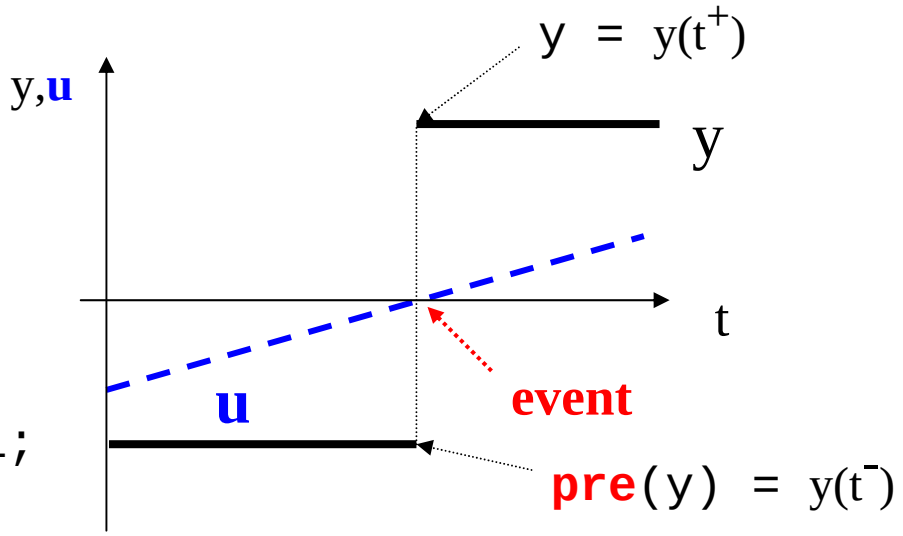


If the switch is open, system is stiff!

Continuous Variables and the if-Statement

- State events
  - zero-crossing function
  - i.e. bi-section method between adjacent time points

```
y = if u>0 then 1 else -1;
```



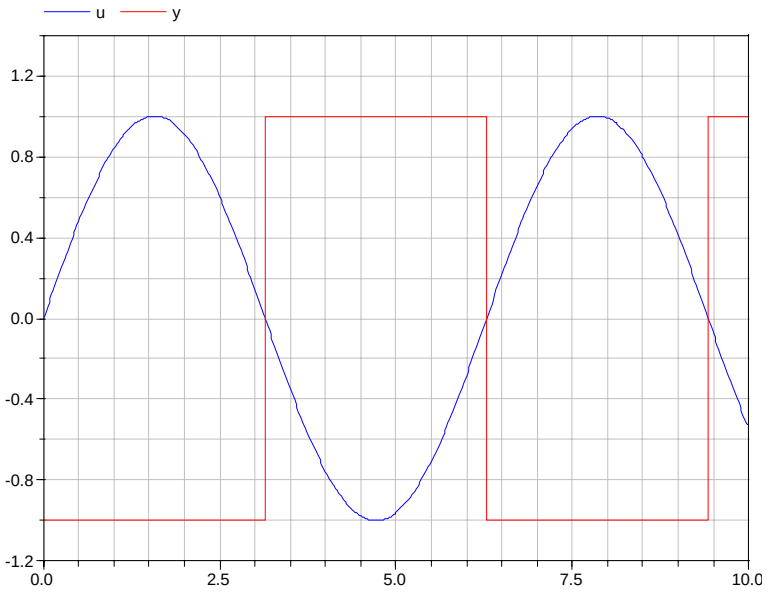
- Time events
  - no zero-crossing function necessary
  - special treatment during compile time possible

```
y = if time>.5 then 1 else -1;
```

Principle Strategy at Events (Simple Example)

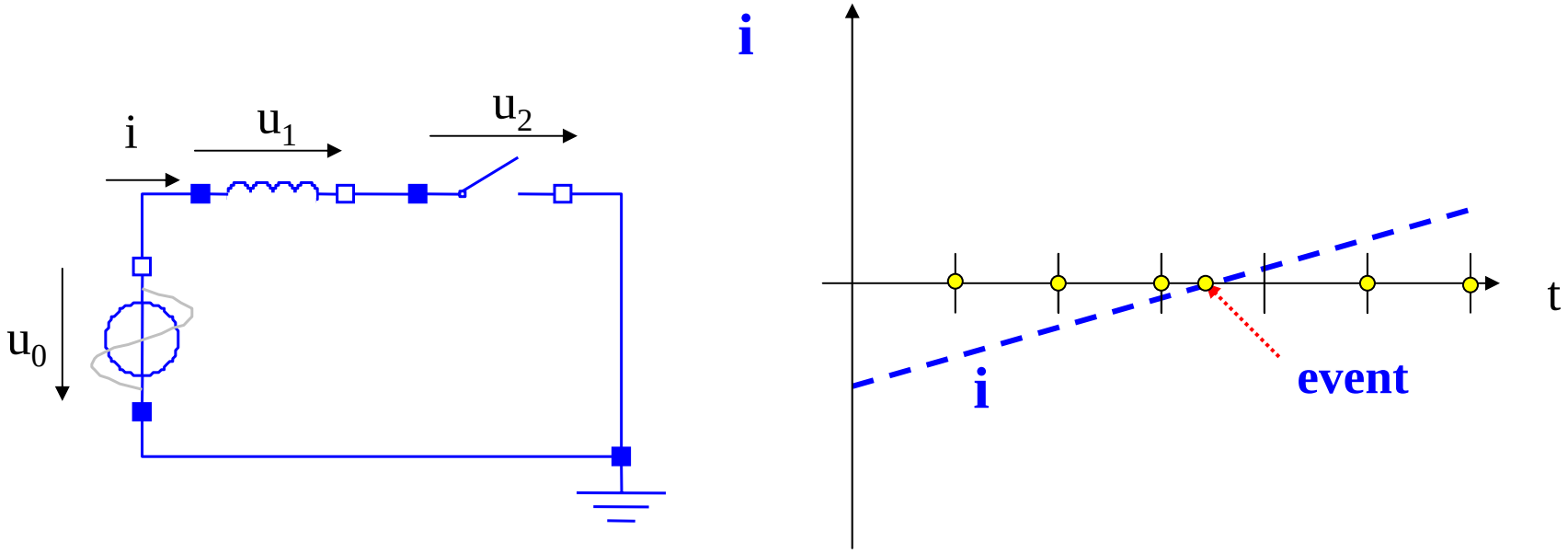
- Standard-solution method
  - Stop integration at event time
  - Do necessary adjustments
    - change input signals and/or discrete variables, re-initialize states
  - Restart integration routine
    - start-up of multi-step methods, initial step-size
- Continuous time integration between events
  - Appropriate step size control
- Store signals twice at event time
  - Variables before and after the event

```
model StateEvent
  import Modelica.Math.sin;
  Real u;
  Real y;
equation
  u = sin(time);
  y = if u<0 then 1 else -1;
end StateEvent
```



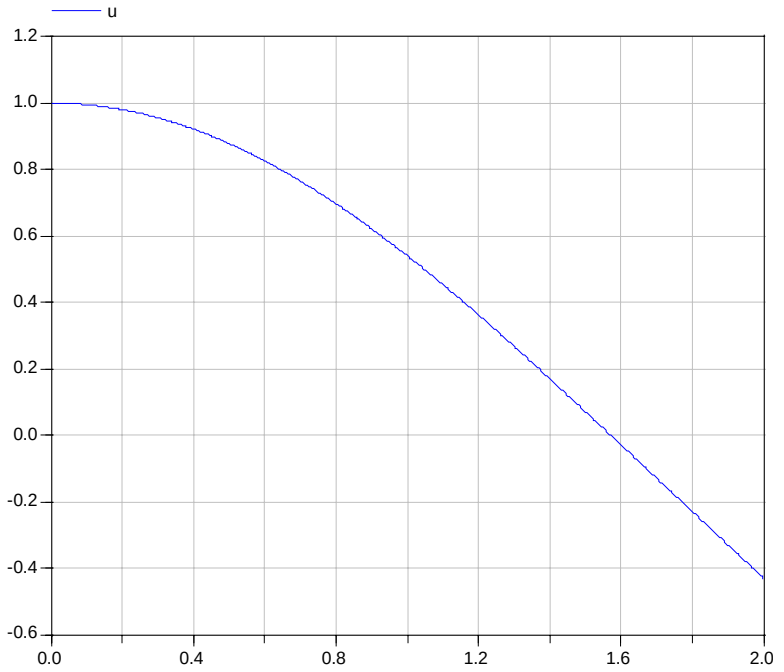
Real-Time Solution to Events

- One-step method with fixed step-size
  - Detect event (u crosses 0)
  - Approximate exact event time
    - use (linear) polynomial approximation of the signal
  - Restart integration routine
    - combine two equidistant steps



Influence Event-Handling

```
model SmoothEvent
  constant Real pi=Modelica.Constants.pi;
  Real x,z,y,u;
equation
  x = if time<pi/2 then cos(time) else pi/2-time;
  y = noEvent( if time<pi/2 then cos(time) else pi/2-time);
  z = smooth(1,if time<pi/2 then cos(time) else pi/2-time);
  u = smooth(1, noEvent(if time<pi/2 then cos(time) else pi/2-time));
end SmoothEvent
```



Semantical interpretation:

- Equation for x: triggers event
- Equation for y: no event handling
- Equation for z: may trigger event
  - may depend on the integration method
- Equation for u: no event handling

Sorting Equations Including if-Equations

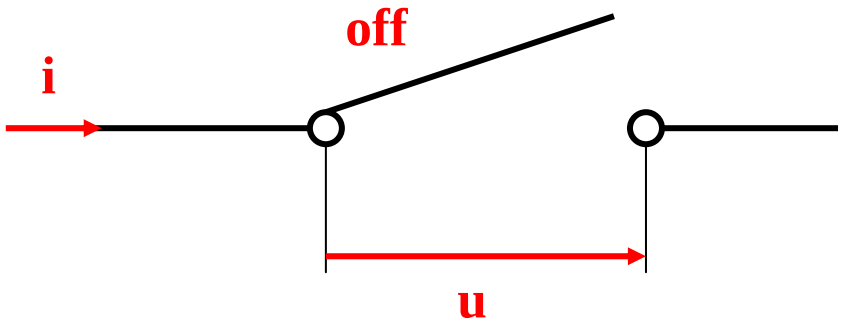
- Modelica model:
  - Differential equations, algebraic equations

$$\underline{0} = \underline{f}\left(t, \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

  - if-equations
    - `y = if <cond> then <expr1> else <expr2>;`
- Mathematical view:
  - `<cond>` c is a boolean expression
    - may depend on a state or time event (Causality)
  - An if-equation is treated as one equation depending on `<cond>` c and the variables $w_1,\ldots w_n$ in `<expr1>` and $v_1, \ldots, v_m$ in `<expr2>`

$$0 = g\left(c, w_1, \ldots, w_n, v_1, \ldots, v_m, \underline{p}\right)$$

Example: Ideal Electrical Switch



The ideal switch is described by the following two equations:

off = true: **i = 0**

off = false: **u = 0**

Corresponding Modelica code:

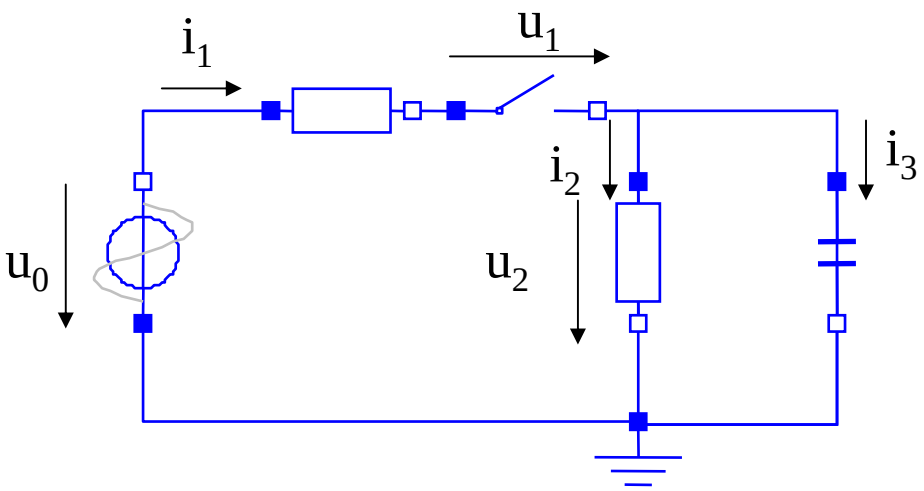
```
0 = if off then i else u;
```

Equivalent description (**off = 0/1**):

$0 = off\ i + (1 - off)\ u$

$\longrightarrow \quad 0 = f(i, u, off)$

Example: Ideal Electrical Switch



$$u_0 = A\sin(\omega t)$$

$$u_0 = R_1 \cdot i_1 + u_1 + u_2$$

$$0 = off \cdot i_1 + (1 - off) \cdot u_1$$

$$i_2 = R_2 / u_2$$

$$i_3 = i_1 - i_2$$

$$C\dot{u}_2 = i_3$$

Linear system of two equations:

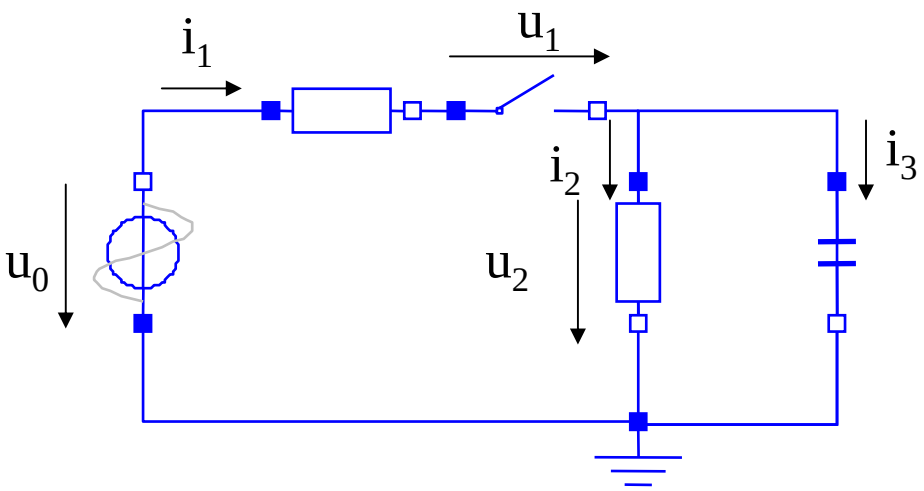
$$\begin{aligned} u_0 &= R_1 \cdot i_1 + u_1 + u_2 \\ 0 &= off \cdot i_1 + (1 - off) \cdot u_1 \end{aligned} \quad \longrightarrow \quad \begin{bmatrix} R_1 & 1 \\ off & (1 - off) \end{bmatrix} \cdot \begin{bmatrix} i_1 \\ u_1 \end{bmatrix} = \begin{bmatrix} u_0 - u_2 \\ 0 \end{bmatrix}$$

Two possible solutions:

$off = 1$: $i_1 = 0$, $u_1 = u_0 - u_2$

$off = 0$: $u_1 = 0$, $i_1 = (u_0 - u_2) / R_1$

Example: Ideal Electrical Switch



$$u_0 = A\sin(\omega t)$$

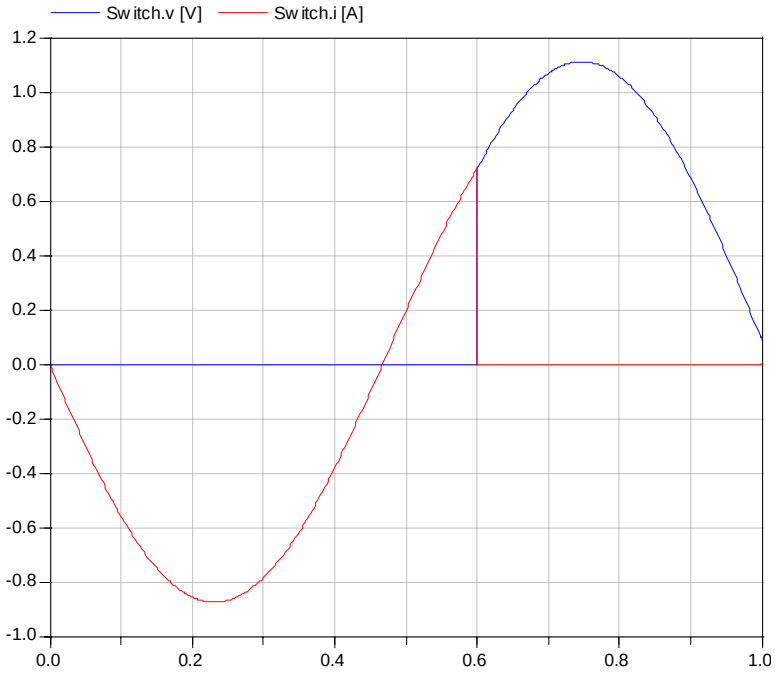
$$u_0 = R_1 \cdot i_1 + u_1 + u_2$$

$$0 = off \cdot i_1 + (1 - off) \cdot u_1$$

$$i_2 = R_2 / u_2$$

$$i_3 = i_1 - i_2$$

$$C\dot{u}_2 = i_3$$

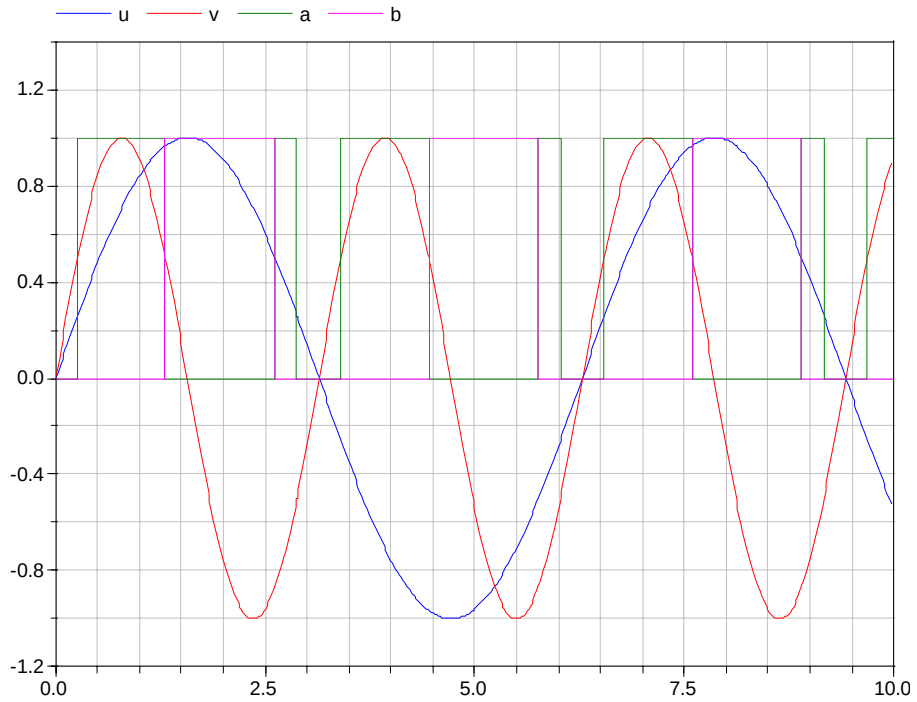


Unrealistic behavior :

- The current can not jump to zero
- Usually an arc keeps current flowing
- Current must be close to zero
- Additional logic necessary
  - needs **when**-equations
    (example will be continued)

Algebraic Loops Involving Integer and/or Boolean Variables

```
model AlgebraicLoopBoolean
  Boolean a(start=true);
  Boolean b;
  Real u;
  Real v;
equation
  u = sin(time);
  v = sin(2*time);
  b = not pre(a) and abs(u)>0.5;
  a = not b and abs(v)>0.5;
end AlgebraicLoopBoolean
```



Algebraic loops involving boolean variables must be handled by the user!

- Break loops using the **pre** operator

Discrete Variables and the when-Statement

Additional equations can be declared at an event using the **when**-statement. These equations are de-activated during the continuous integration.

```
when  <condition>  then
   <equations>
end when;
```

When <condition> becomes true, <equations> are calculated.

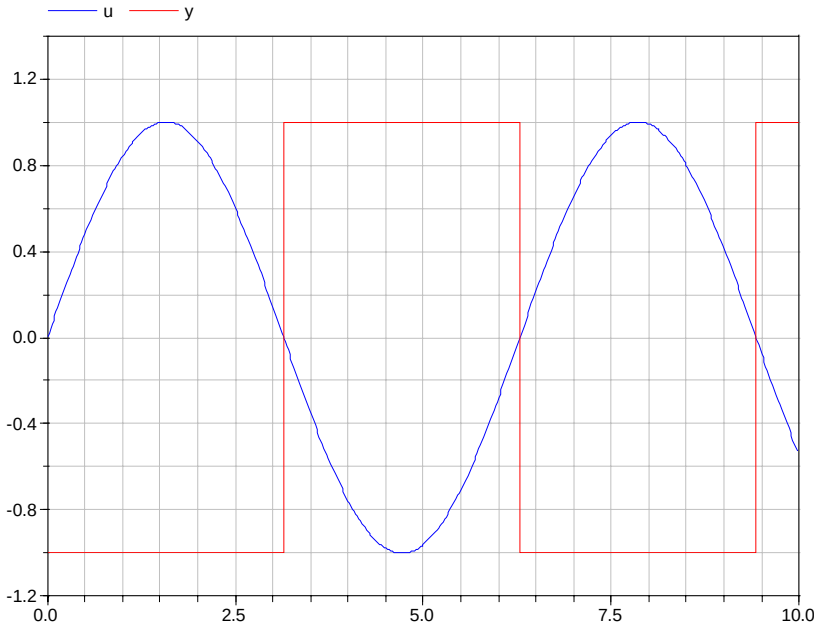
Equivalent formulation:

```
if edge(<condition>)  then
    <equations>
end if;
```

<condition> may not depend on a **noEvent()** Operator. Therefore, only at event points the equations within the when clause are evaluated

Re-writing State Events to Time Events

```
model HandleEvents
  constant Real PI=Modelica.Constants.pi;
  Real u;
  Real y;
  Boolean flag(start=false);
equation
  u = Modelica.Math.sin(time);
  when sample(PI,PI) then
    flag = not pre(flag);
  end when;
  y = if flag then 1 else -1;
//y = if u<0  then 1 else -1;
end HandleEvents
```



Real-time efficiency:

- If possible use time-events instead of state-events

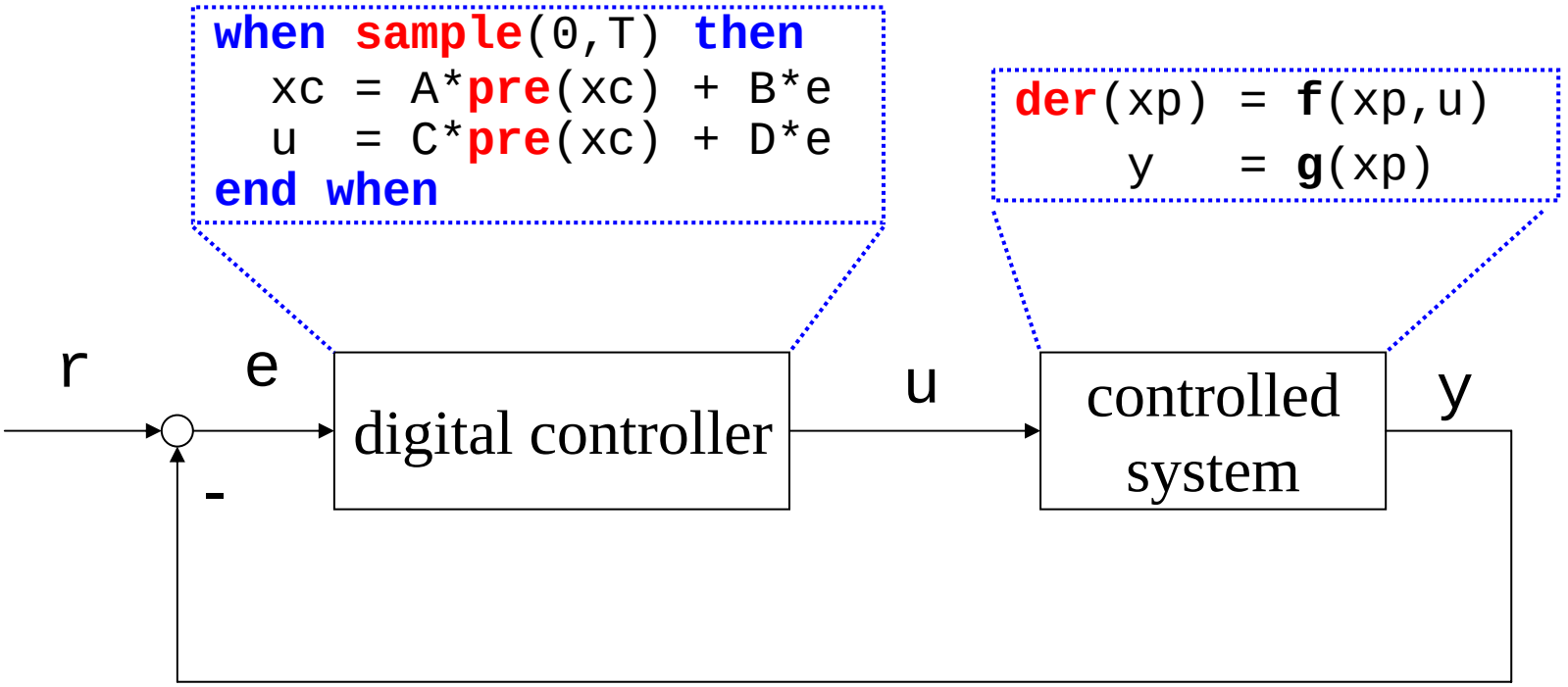
Sorting Equations Including when-Statements

- Modelica model:
  - Differential equations, algebraic equations, and if-equations

$$\underline{0} = \underline{f}\left(t, \underline{\dot{x}}(t), \underline{x}(t), \underline{y}(t), \underline{u}(t), \underline{p}\right)$$

  - Discrete equations only active at events
    - `when <cond> then <equations> end when;`
- Mathematical view:
  - Same number of equations and unknowns at each time point
  - Different number of equations and unknowns during event
- Algorithmic strategy:
  - Sorting is based on all equations

Example: Digital Controller




```
y := g(xp);
e := r - y;
when sample(0,T) then
  xc := A*pre(xc) + B*e;
  y  := C*pre(xc) + D*e;
end when
der(xp) := f(xp,u);
```

Order of evaluation is correct for the sample time points as well as during continued time integration!

(xp and **pre**(xc) are known)

Sorting Equations of Hybrid Models

- IMPORTANT:
  Each discrete variable is determined by one equation
  - Example:

```
when h1>0 then
   openValve = true;
end when;


when h2<2 then
   openValve = false;
end when;
```

  - Not allowed since two equations for one variable `openValve`
  - Combine conditions `h1>0` and `h2<2`

Sorting Equations of Hybrid Models

Re-writing event equations

```
when h1>0 or h2<2 then
   openValve = if edge(h1 > 0) then true else false;
end when;
```

Semantical interpretation:

If one condition becomes true, (i.e. `h1 > 0`), no further event will happen not even when the second condition (`h2 < 2`) becomes true.

Boolean expression (`h1>0 or h2<2`) will not change anymore!

This is not the desired logic!

Sorting Equations of Hybrid Models

Desired logic can be described by

```
when {h1>0, h2<2}  then
  openValve = if edge(h1 > 0) then true else false;
end when;
```

or even shorter:

```
when {h1>0, h2<2}  then
  openValve = edge(h1 > 0);
end when;
```

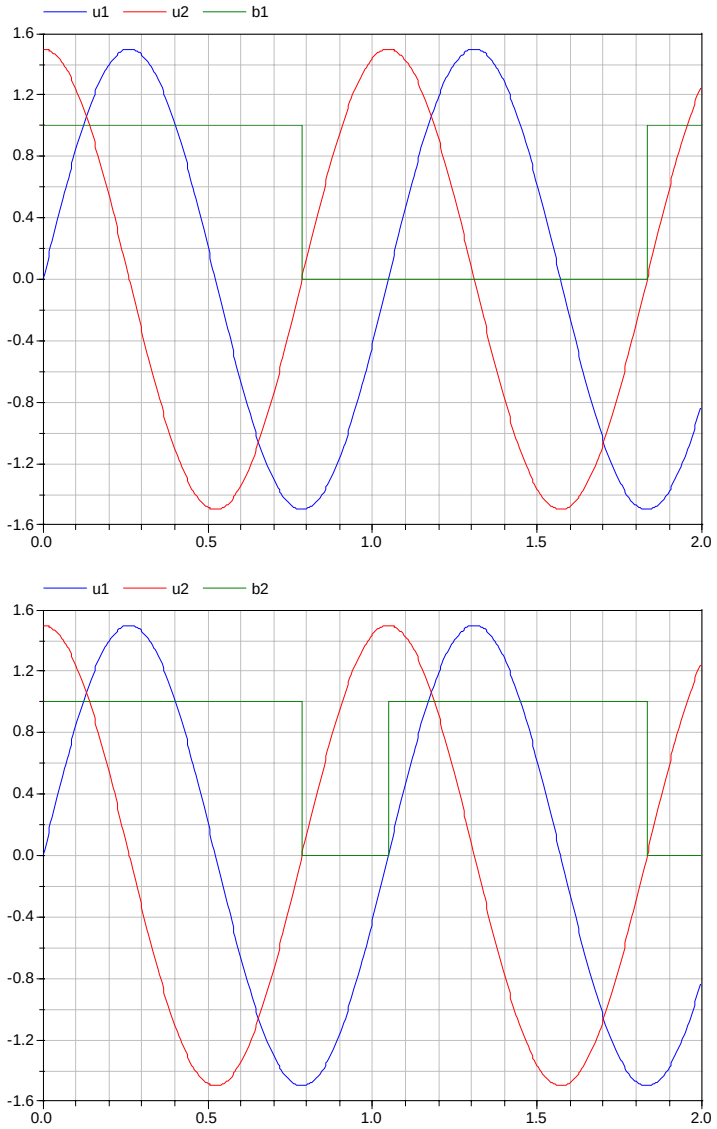
```
when {expr1, expr2, expr3, ...} then
```

Semantical interpretation:

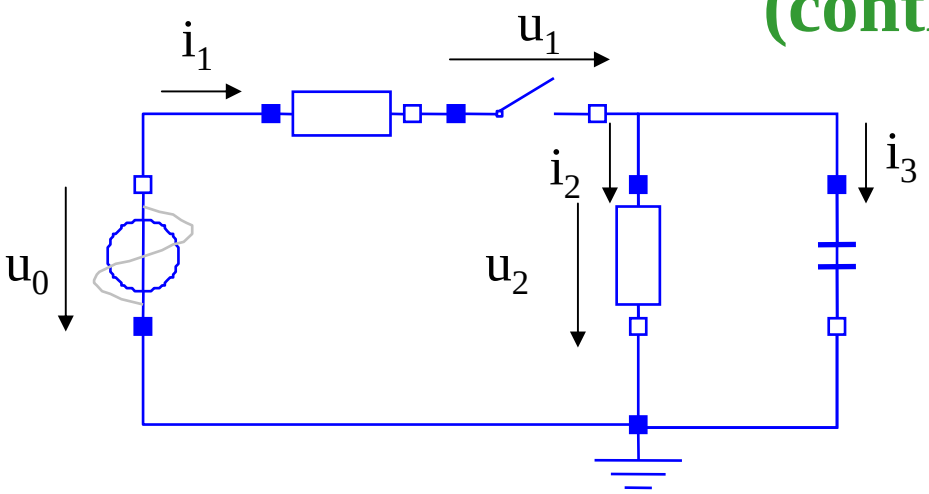
- Triggers an event, if one of the listed boolean expression becomes true

Example: Difference of „or“ and {...,...}

```
model whendemo3
    parameter Real A=1.5, w=6;
    Real    u1, u2;
    Boolean b1, b2;
equation
    u1 = A*sin(w*time) + 1.e-10;
    u2 = A*cos(w*time);
    when u1 > 0 or u2 > 0 then
        b1 = not pre(b1);
    end when;
    when {u1 > 0, u2 > 0} then
        b2 = not pre(b2);
    end when;
end whendemo3;
```



Example: Ideal Electrical Switch (continued)



$$u_0 = A\sin(\omega t)$$

$$u_0 = R_1 \cdot i_1 + u_1 + u_2$$

$$0 = off \cdot i_1 + (1 - off) \cdot u_1$$

$$i_2 = R_2 / u_2$$

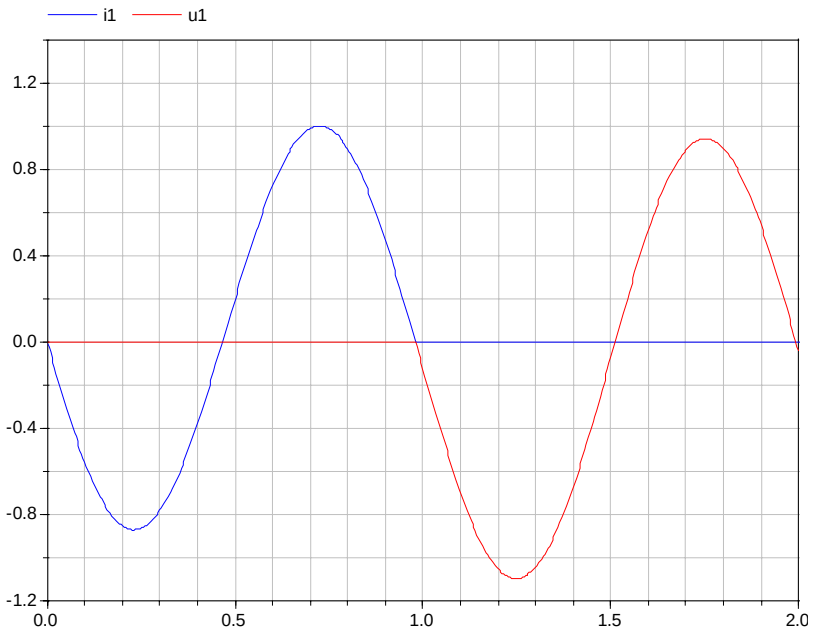
$$i_3 = i_1 - i_2$$

$$C\dot{u}_2 = i_3$$

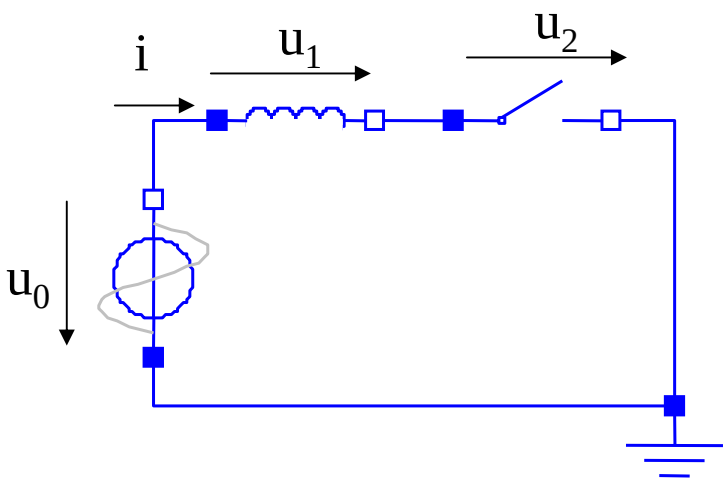
Introduce additional logic :

- Algebraic loop with boolean variable

```
when (time>t0) then
  sign_i = if (i1>0) then 1 else -1;
end when;
when (time>t0 and sign_i*i1<0) then
  off = true;
end when;
0 = if pre(off) then i1 else u1;
```



Example: Ideal Electrical Switch (continued)

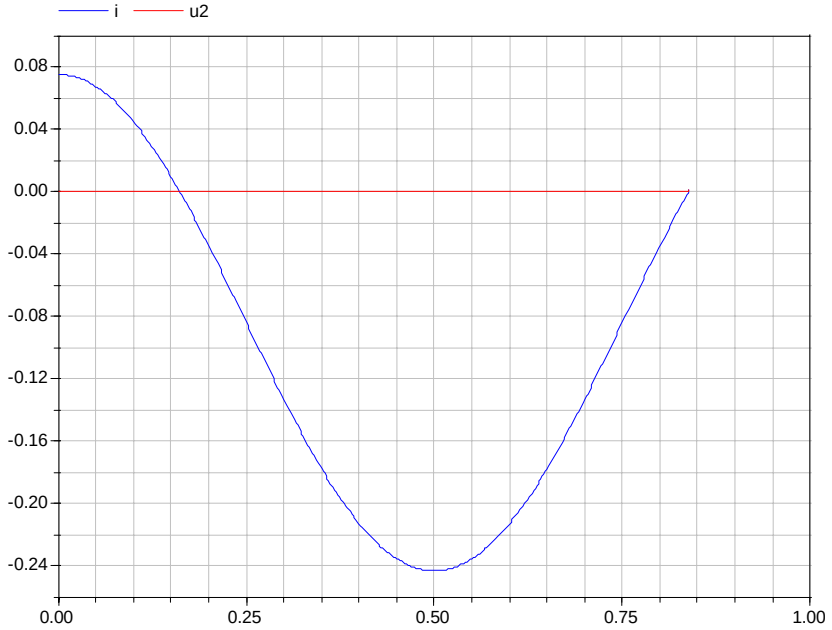


$$u_0 = A\sin(\omega t)$$

$$0 = off \cdot i + (1 - off) \cdot u_2$$

$$L\frac{di}{dt} = u_1$$

$$u_0 = u_1 + u_2$$



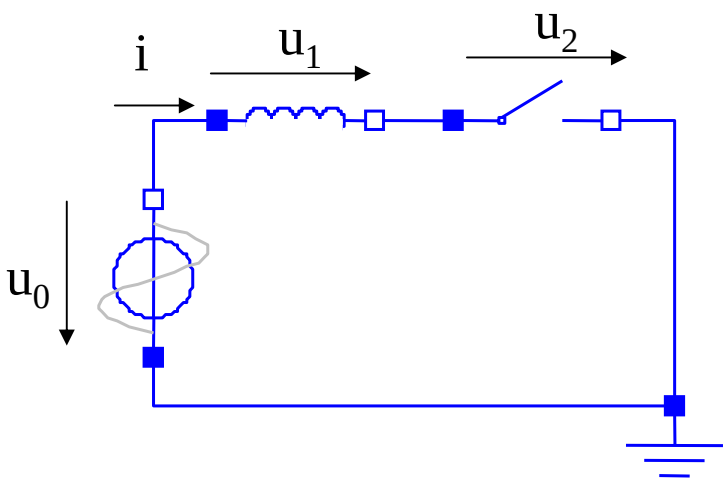
Causality (off = 0/1):

- i is a state and is therefore known

$$u_2 = \frac{-off \cdot i}{1 - off}$$

Only solvable, iff *off*=0

Example: Ideal Electrical Switch (continued)



$$u_0 = A\sin(\omega t)$$

$$0 = off \cdot \frac{di}{dt} + (1 - off) \cdot u_2$$

$$L\frac{di}{dt} = u_1$$

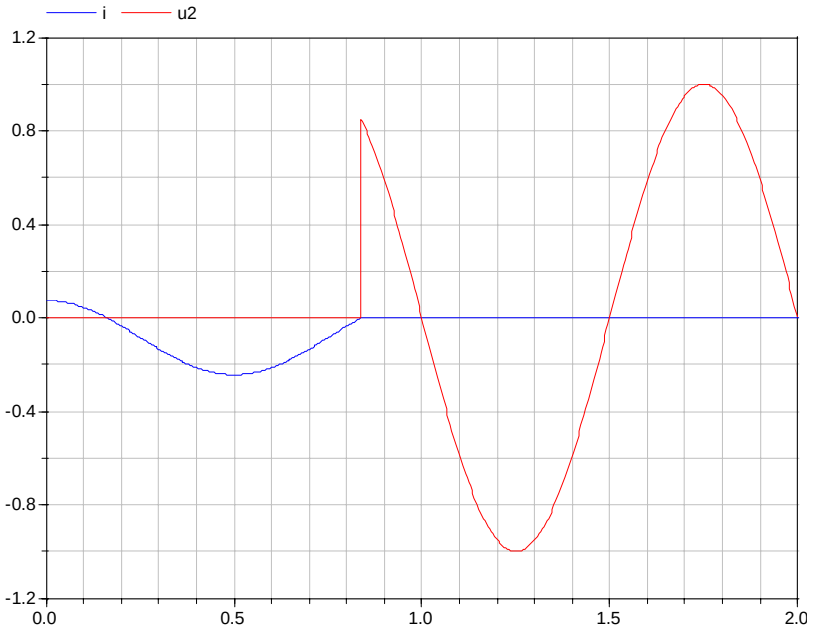
$$u_0 = u_1 + u_2$$

Varying higher-index problem

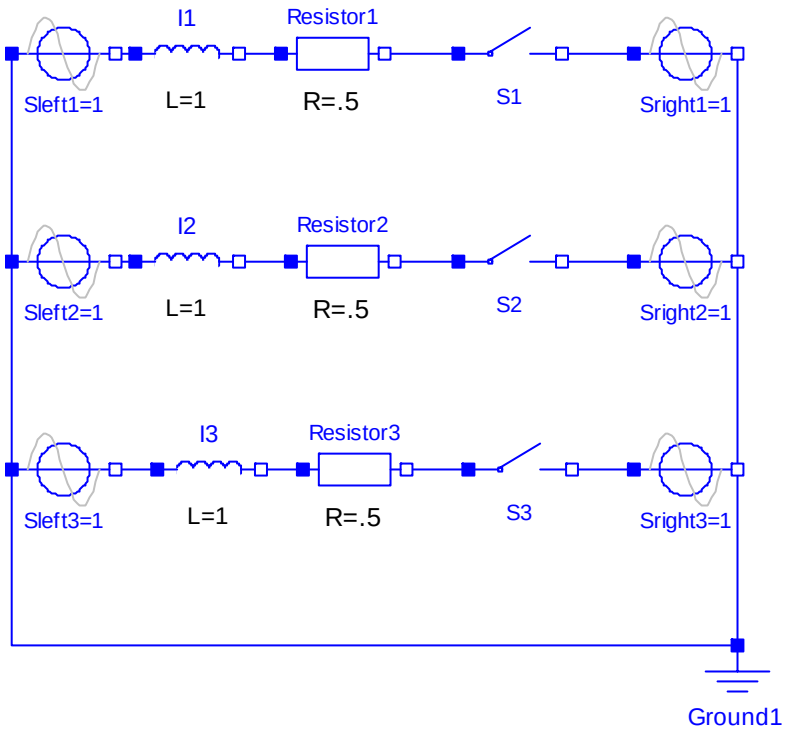
$off = 0 \quad : \quad u_2 = 0$ index=1

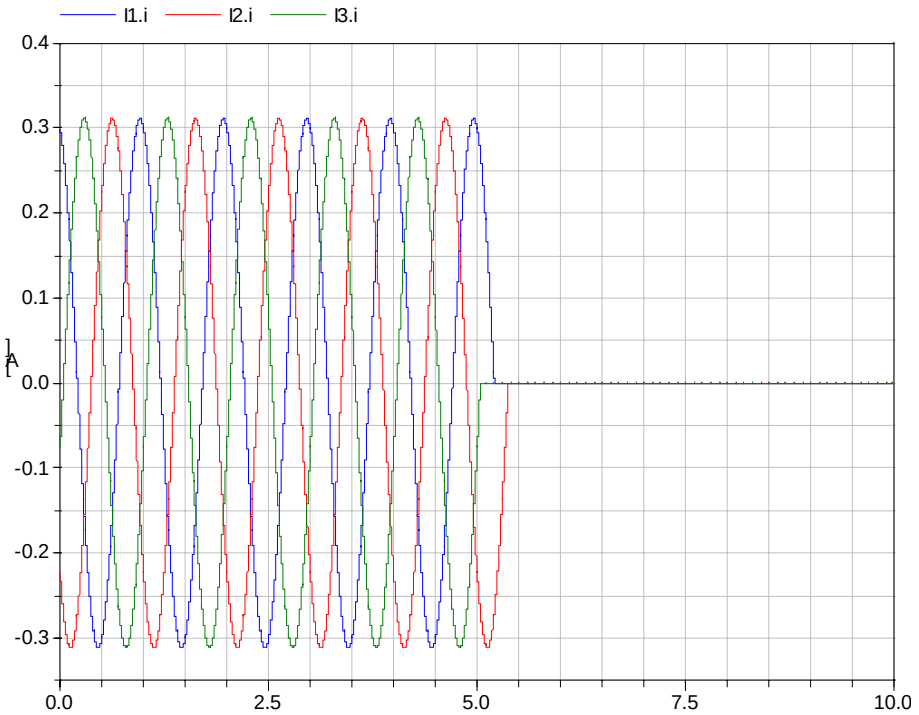
$off = 1 \quad : \quad i = 0$ index=2

$$\frac{di}{dt} = 0$$



Example: 3-Phase Electrical System (continued)



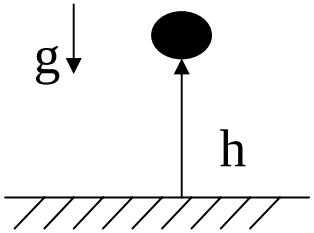


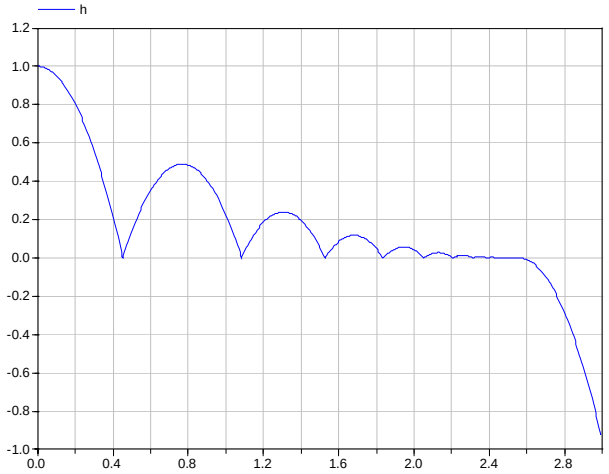
Switch works also for the 3-Phase electrical system

- Introducing dq0-reference frame still very efficient
- `i_dq0` used as state
- Initialization: `der(i_dq0)={0,0,0};`

Numerical Issues

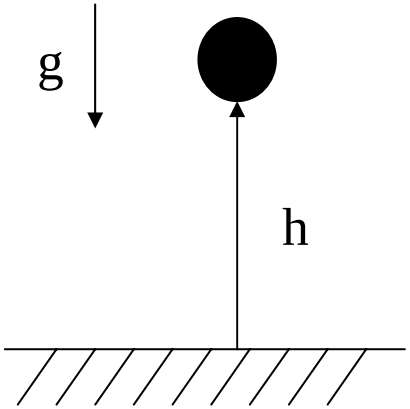
- Standard-solution method
  - Stop integration at event time
  - Do necessary adjustments
  - Restart integration routine
- Due to numerical errors the system can get into a non-physical state
  - Height h is negative in the bouncing ball example
- Solution to this problem
  - Changes in the settings (accuracy) for the solver routine may help
  - Different integration methods may lead to different results
  - Adapt logic to circumvent numerical problems (**Most Efficient**)

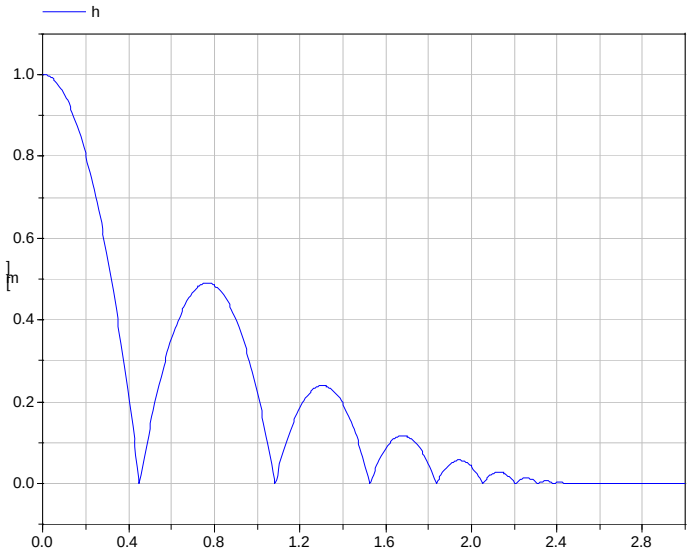





```
model bouncingBall
  parameter Real e=0.7;
  parameter Real g=9.81;
  Real h(start=1);
  Real v;
equation
  der(h) = v;
  der(v) = -g;
  when h < 0 then
    reinit(v, -e*pre(v));
  end when;
end bouncingBall;
```

Numerical Issues
Solution to the Bouncing Ball






```
model bouncingBall
  parameter Real e=0.7;
  parameter Real g=9.81;
  Real h(start=1);
  Real v;
  Boolean flying(start=true)
  Boolean impact;
  Real v_new;
equation
  der(h) = v;
  der(v) = if flying then -g else 0;
  impact = h < 0;
  when {impact,h < 0 and v < 0} then
    v_new = if edge(impact) then -e*pre(v)
                            else 0;
    flying = v_new > 0;
    reinit(v, v_new);
  end when;
end bouncingBall;
```